

UNIVERSITÀ  
DEGLI STUDI  
DI PADOVA

# Introduction to Simulink

## Simulation of nonlinear and hybrid-time systems

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4 Marzo 2024



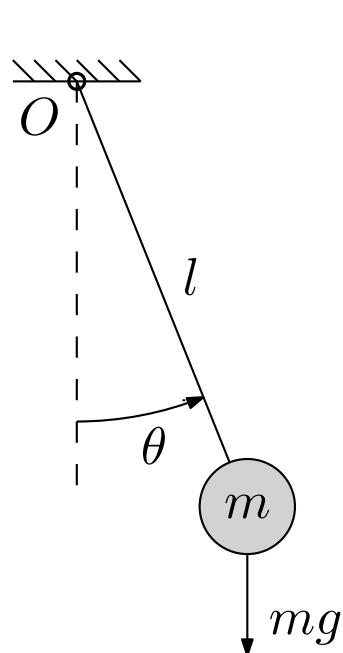
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# Outline

- Simulation of a *nonlinear system*:
  - Modelling of the nonlinear pendulum.
  - Simulation using Lord Kelvin's scheme.
  - Period of the undamped nonlinear pendulum.
  - Comparison with the linearized model.
- Simulation of a *hybrid-time system*:
  - Continuous-time speed PI control of a DC motor.
  - Discrete-time speed PI control loop of a DC motor.

# Simulation of nonlinear systems

Example: simulate the natural response of a simple pendulum, starting from given ICs.



Newton-Euler 2<sup>nd</sup> law

$$J \ddot{\theta} = \sum_n \tau_n$$

Moment of Inertia

$$J = m l^2$$

Nonlinear ODE

Torque due to weight

$$\tau_1 = -mgl \sin \theta$$

Friction torque

$$\tau_2 = -b \dot{\theta}$$

$$ml^2 \ddot{\theta} + b \dot{\theta} + mgl \sin \theta = 0$$

# Simulation of nonlinear systems

Nonlinear ODE (implicit form)

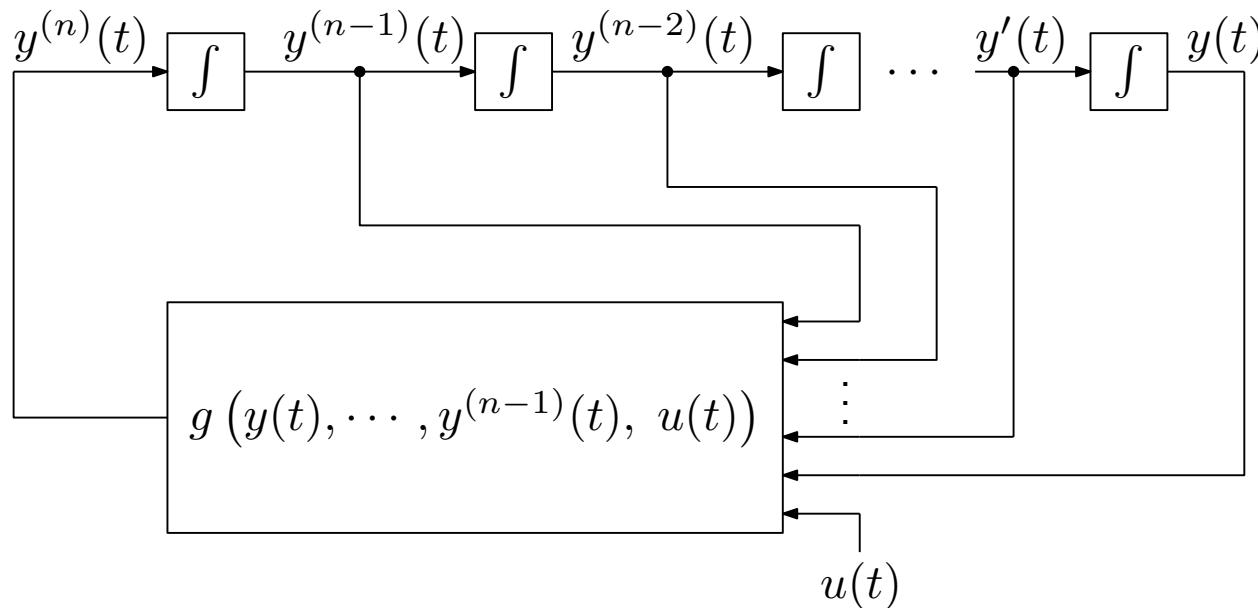
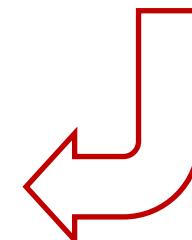
$$f \left( y(t), \dots, y^{(n-1)}(t), y^{(n)}(t), u(t) \right) = 0$$



Nonlinear ODE (explicit form)

$$y^{(n)}(t) = g \left( y(t), \dots, y^{(n-1)}(t), u(t) \right)$$

Lord Kelvin's scheme (chain of integrators)



# Simulation of nonlinear systems

Nonlinear ODE (implicit form)

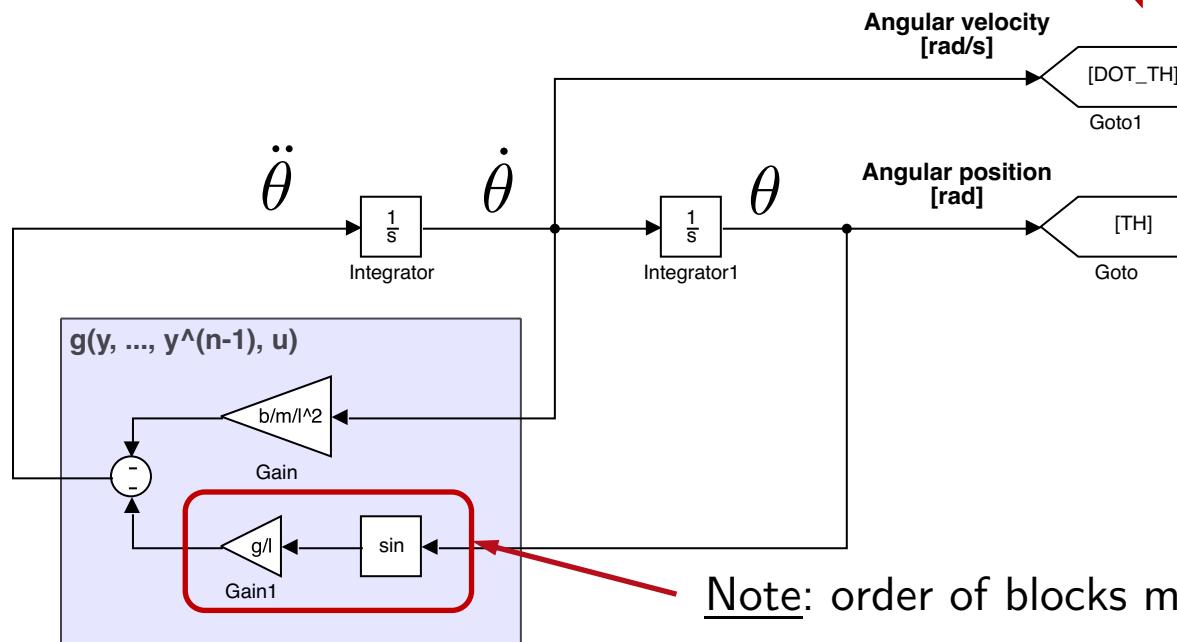
$$ml^2 \ddot{\theta} + b \dot{\theta} + mgl \sin \theta = 0$$



Nonlinear ODE (explicit form)

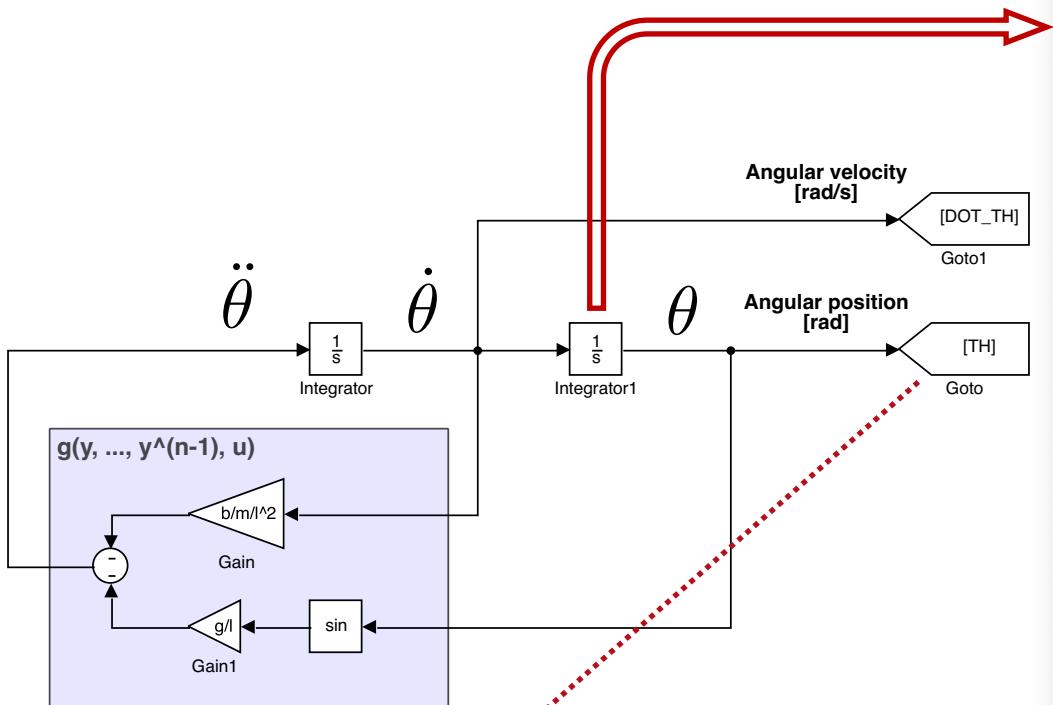
$$\ddot{\theta} = -\frac{b}{ml^2} \dot{\theta} - \frac{g}{l} \sin \theta$$

Lord Kelvin's scheme (chain of integrators)

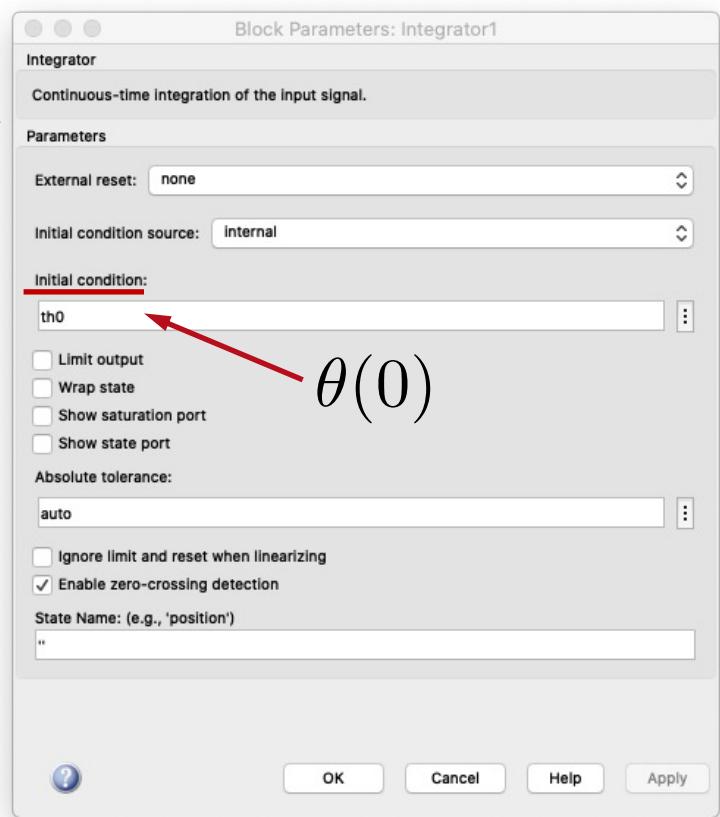
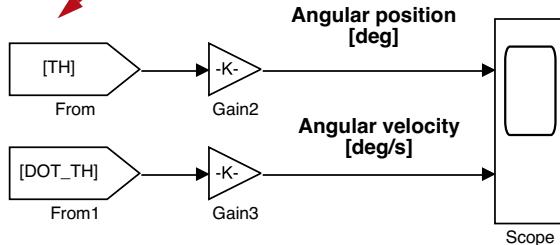


Note: order of blocks matters !

# Simulation of nonlinear systems



A **Goto** block propagates a signal of the **From** block with same label.



Initial state is set in the initial conditions (ICs) of the integrators.

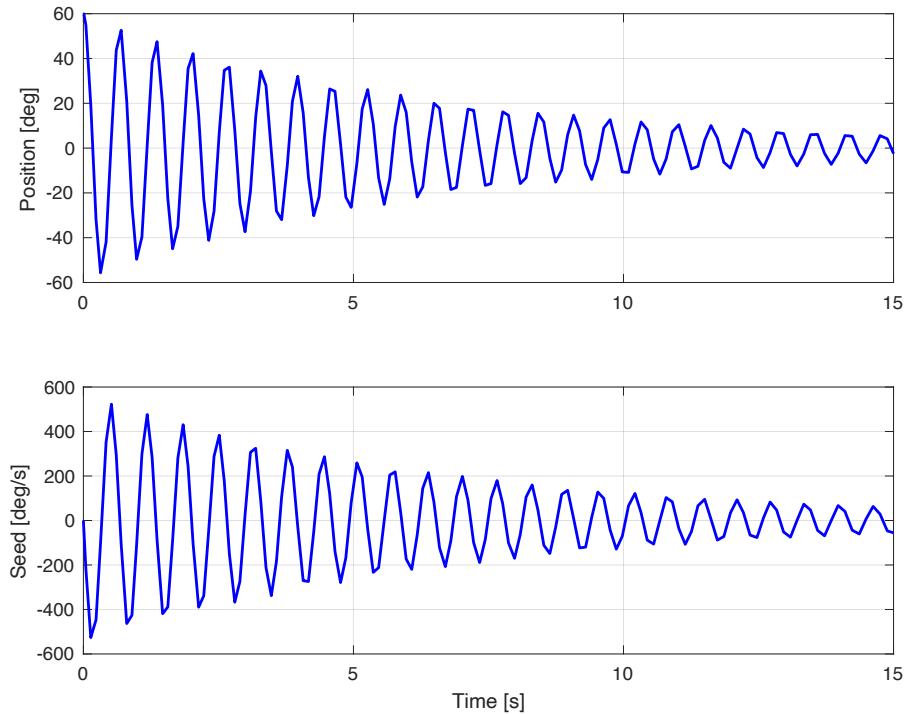
# Simulation of nonlinear systems

Natural response with  $\theta(0) = 60^\circ$ ,  $\dot{\theta}(0) = 0$ .

```
% set simulation parameters
set_param('nonlin_pend', ...
    'SolverType', 'Variable-step', ...
    'Solver', 'ode45', ...
    'MaxStep', 'auto', ...
    'MinStep', 'auto', ...
    'AbsTol', 'auto', ...
    'RelTol', '1e-3', ...
    'StopTime', '15');

% initial conditions
th0 = 60 * deg2rad;
dot_th0 = 0;

% run simulation
sim('nonlin_pend');
```



Max step too large  $\Rightarrow$  reduce max step size ...

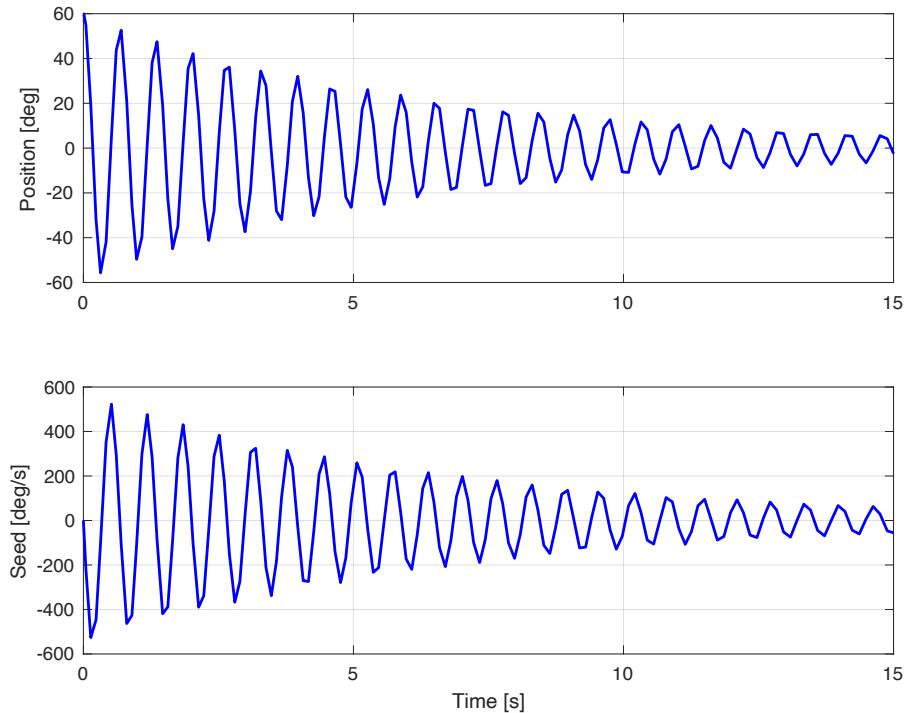
# Simulation of nonlinear systems

Simulation with reduced max step size:

```
% set simulation parameters
set_param('nonlin_pend', ...
    'SolverType', 'Variable-step', ...
    'Solver', 'ode45', ...
    'MaxStep', 'auto', ...
    'MinStep', 'auto', ...
    'AbsTol', 'auto', ...
    'RelTol', '1e-3', ...
    'StopTime', '15');

% initial conditions
th0 = 60 * deg2rad;
dot_th0 = 0;

% run simulation
sim('nonlin_pend');
```

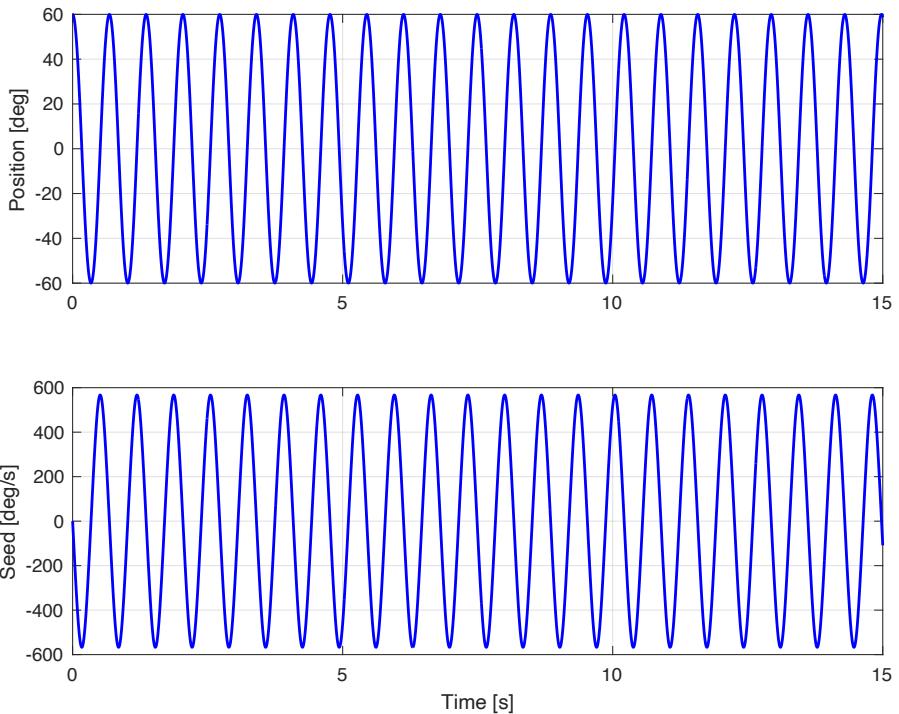


⇒ By increasing the number of integration instants, the response is smoother.

# Simulation of nonlinear systems

Natural response with  $b = 0$  (*undamped sys*):

```
% set damping to zero  
b = 0;  
  
% run simulation  
sim('nonlin_pend');
```

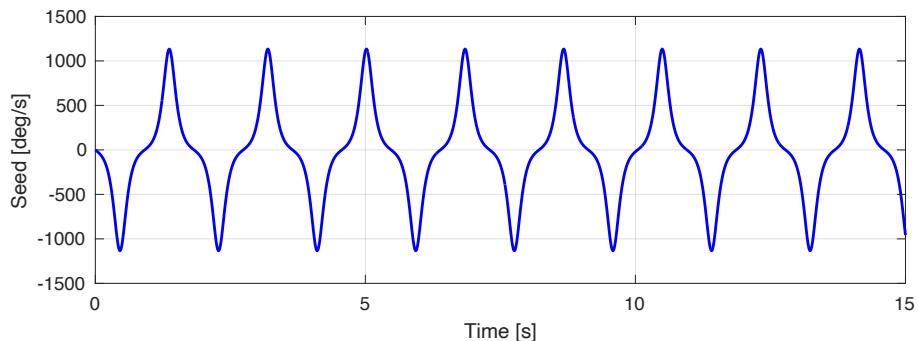
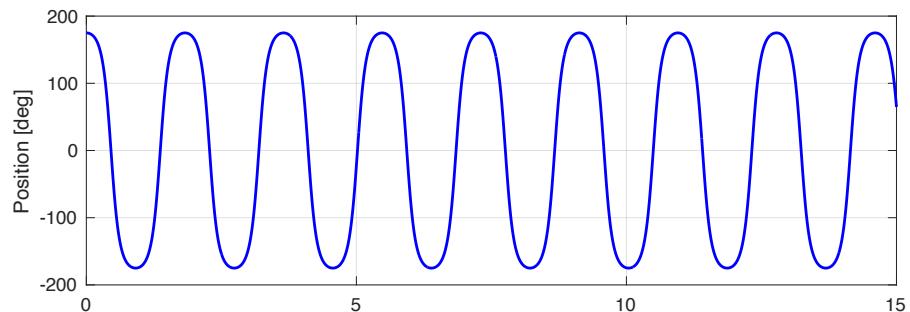


⇒ With no damping (no energy dissipation), the response is periodic.

# Simulation of nonlinear systems

The oscillation is not *harmonic* (i.e. not a pure sinusoidal motion). This is more noticeable for large swings ( e.g.  $\theta(0) = 175^\circ$ ,  $\dot{\theta}(0) = 0$  ).

```
% initial conditions  
th0 = 175 * deg2rad;  
dot_th0 = 0;  
  
% run simulation  
sim('nonlin_pend');
```



# Simulation of nonlinear systems

For an *undamped* nonlinear pendulum with  $\theta(0) = \theta_0$  and  $\dot{\theta}(0) = 0$ , the period of the oscillation is equal to <sup>(1,2)</sup>:

$$T = 4 \sqrt{\frac{l}{g}} K \left( \sin \frac{\theta_0}{2} \right)$$

where:

$$K(m) = \int_0^{\pi/2} \frac{d\theta}{\sqrt{1 - m^2 \sin^2 \theta}}$$

Elliptical integral  
of the 1<sup>st</sup> kind

(1) <https://www.math24.net/nonlinear-pendulum/>

(2) <http://www.sciencedirect.com/science/article/pii/S089812211200017X>

# Simulation of nonlinear systems

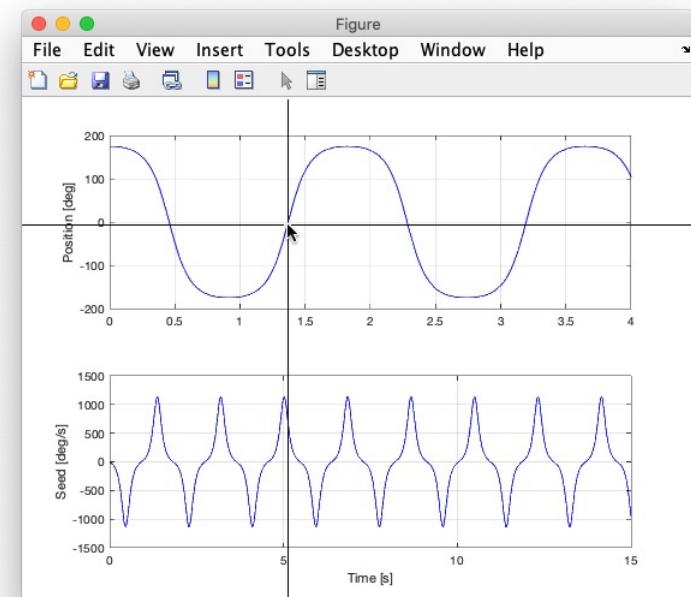
```
% period of the nonlinear pendulum  
k = sin(theta/2);  
K = ellipke(k^2);  
T_nlin = 4*sqrt(l/g)*K  
  
T_nlin = 1.8255
```

Note: the **ellipke** routine evaluates the elliptical integral of the 1<sup>st</sup> kind in the form:

$$K(m') = \int_0^{\pi/2} \frac{d\theta}{\sqrt{1 - m' \sin^2 \theta}}$$

Check the result by measuring the period on the plot with the **ginput** command ...

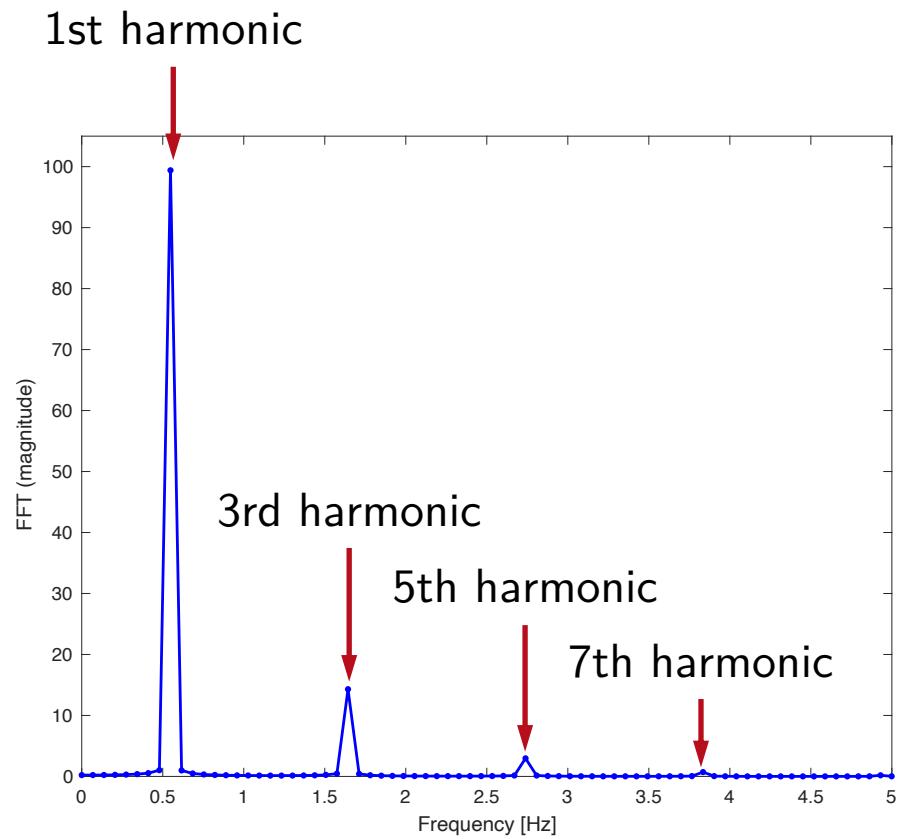
```
Command Window  
New to MATLAB? See resources for Getting Start  
>> ginput  
  
ans =  
  
1.3779 -4.1667  
3.1935 -4.1667  
  
>> diff(ans(:,1))  
  
ans =  
  
1.8157  
  
fx >>
```



# Simulation of nonlinear systems

Spectrum (FFT) of the nonlinear oscillation:

```
% select final time to consider  
% an integer number of periods  
t1f = T_nlin * floor(t(end)/T_nlin);  
  
% resample at fixed rate  
Ts = T_nlin/100;  
t1 = 0:Ts:t1f;  
th1 = interp1(t, th, t1);  
  
% compute fft  
Fs = 1/Ts;  
N1 = length(t1);  
f1 = linspace(0, Fs, N1);  
  
th1_fft = (1/N1)*fft(th1);
```

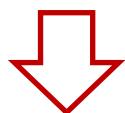


# Simulation of nonlinear systems

For small oscillations, the dynamics can be *linearized* with the approximation  $\sin \theta \approx \theta$ :

Nonlinear ODE

$$ml^2 \ddot{\theta} + b \dot{\theta} + mgl \sin \theta = 0$$



$$\sin \theta \approx \theta$$

Linearized ODE

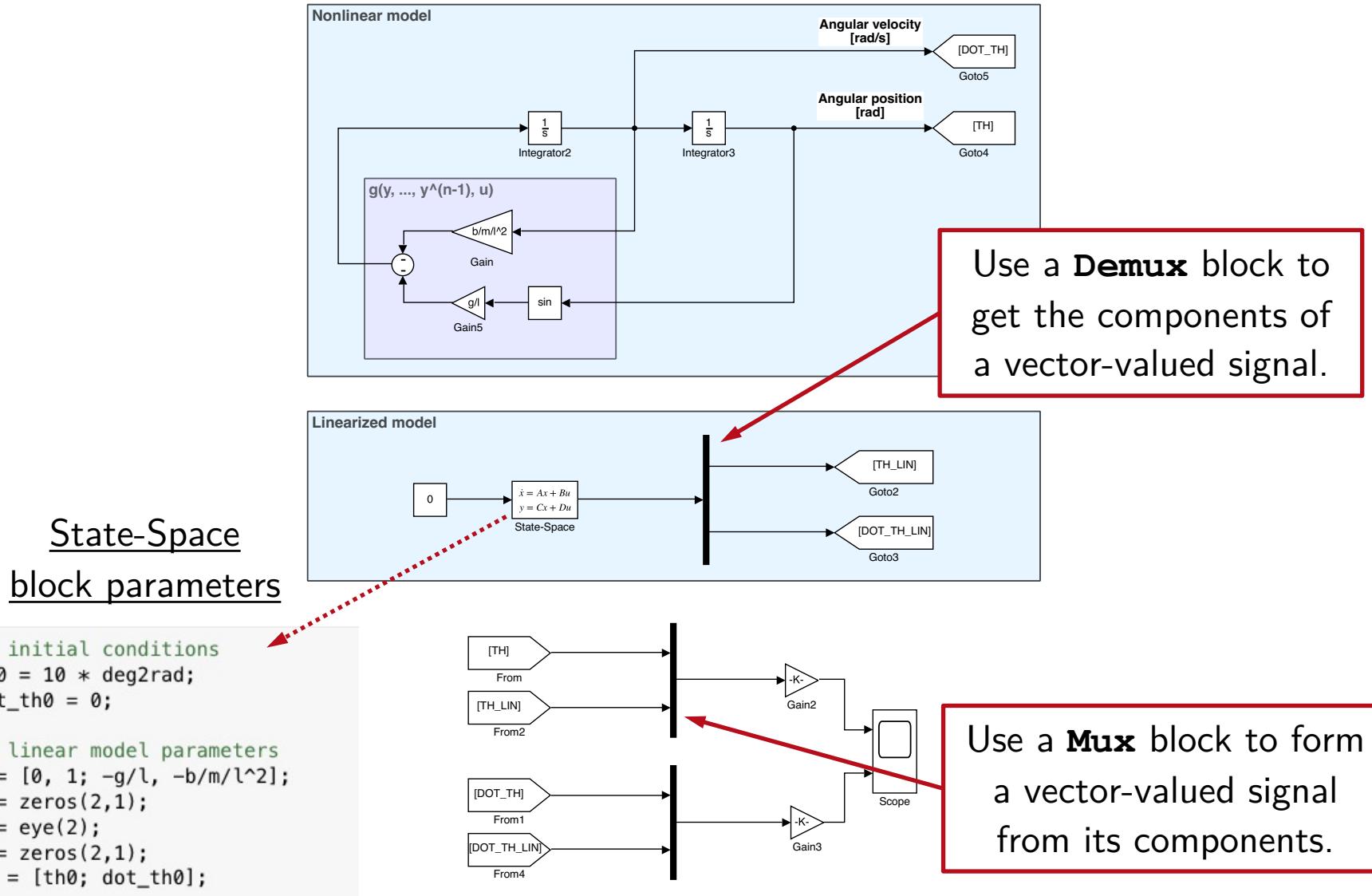
$$ml^2 \ddot{\theta} + b \dot{\theta} + mgl \theta = 0$$



Linear state-space model

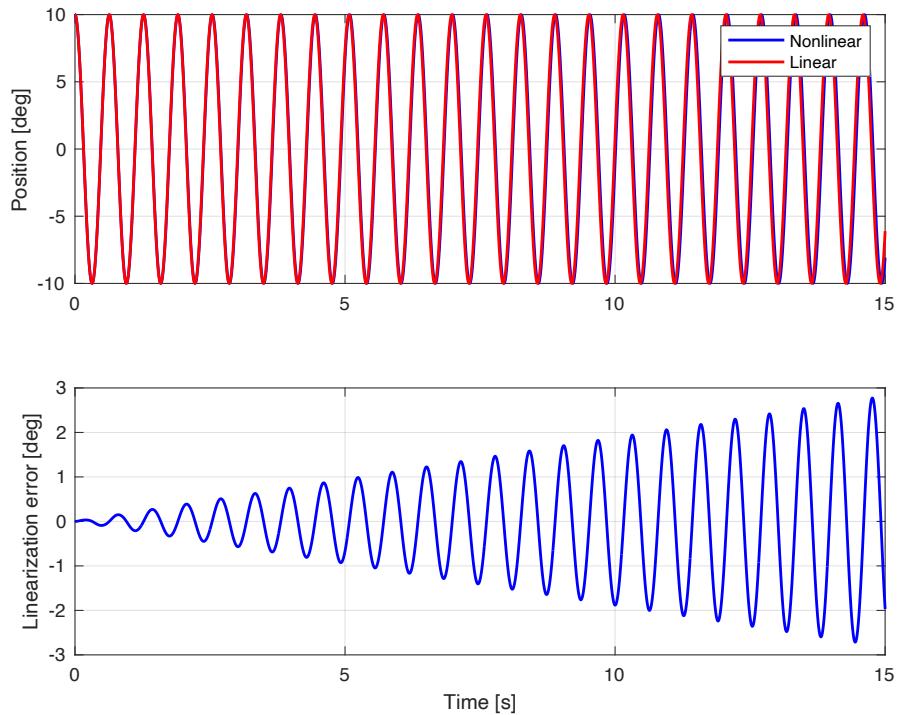
$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{l} & -\frac{b}{ml^2} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$$

# Simulation of nonlinear systems



# Simulation of nonlinear systems

```
% set simulation parameters  
set_param('nonlin_vs_lin_pend', ...  
    'SolverType', 'Variable-step', ...  
    'Solver', 'ode45', ...  
    'MaxStep', '0.01', ...  
    'MinStep', 'auto', ...  
    'AbsTol', 'auto', ...  
    'RelTol', '1e-3', ...  
    'StopTime', '15');  
  
% run simulation  
sim('nonlin_vs_lin_pend');
```



The two oscillations are not identical; in particular, their periods are slightly different ...

# Simulation of nonlinear systems

The undamped linearized pendulum is an *harmonic oscillator*:

Linearized ODE (with  $b = 0$ )

$$ml^2 \ddot{\theta} + b \dot{\theta} + mgl \theta = 0 \quad \rightarrow \quad \ddot{\theta} + \omega_0^2 \theta = 0, \quad \omega_0 = \sqrt{\frac{g}{l}}$$

The period of the oscillation is:

$$T_l = \frac{2\pi}{\omega_0} = 2\pi \sqrt{\frac{l}{g}}$$

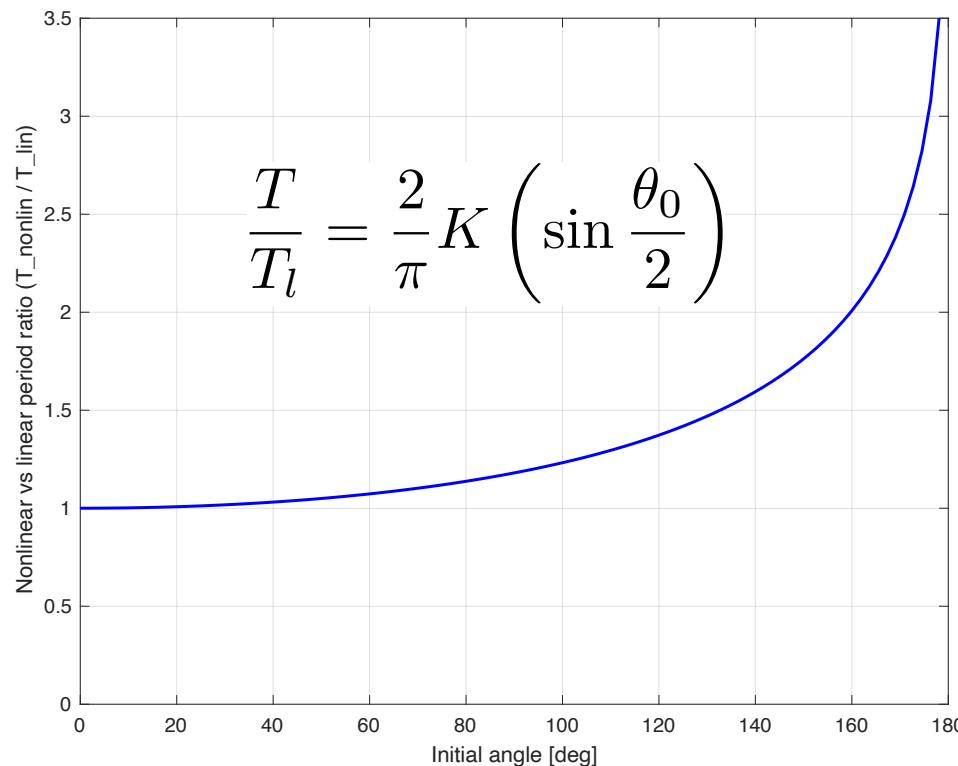
# Simulation of nonlinear systems

Nonlinear undamped pendulum

$$T = 4\sqrt{\frac{l}{g}} K \left( \sin \frac{\theta_0}{2} \right)$$

Linear undamped pendulum

$$T_l = 2\pi\sqrt{\frac{l}{g}}$$



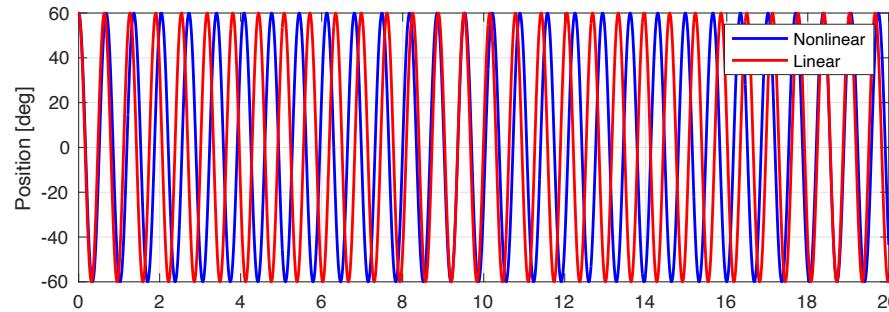
# Simulation of nonlinear systems

The linearization error is:

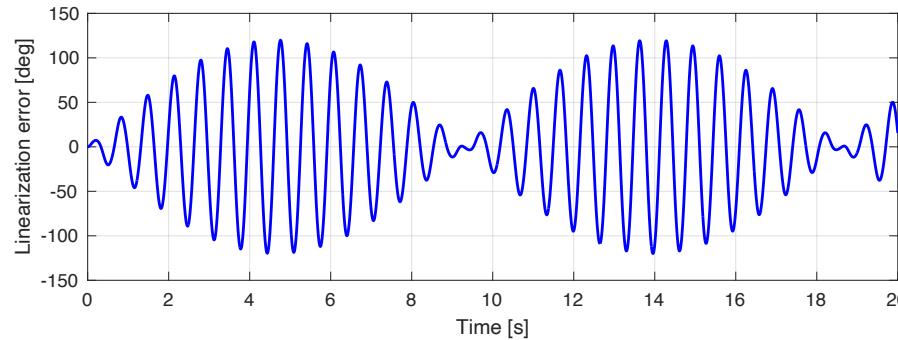
$$e(t) = \theta_0 (\cos \omega t - \cos \omega_l t) + \text{H.O.H.}$$

$$= -2\theta_0 \sin\left(\frac{\omega - \omega_l}{2} t\right) \sin\left(\frac{\omega + \omega_l}{2} t\right) + \text{H.O.H.}$$

High Order Harmonics



$$\begin{aligned}\theta(0) &= 60^\circ \\ \dot{\theta}(0) &= 0\end{aligned}$$



# Simulation of a sampled-data system

Example: consider the following simplified model of a DC motor:

$$P(s) = \frac{Y(s)}{U_a(s)} = \frac{k}{T s + 1}, \quad k = 8.3, \quad T = 0.028$$

with the armature voltage  $u_a$  [V] as input, and the shaft speed  $y$  [rad/s] as output.

Want to simulate the response of a speed PI control loop, assuming to directly measure the shaft speed (e.g. by using a *tachometer*).

# Simulation of a sampled-data system

Start with the *continuous-time* PI controller:

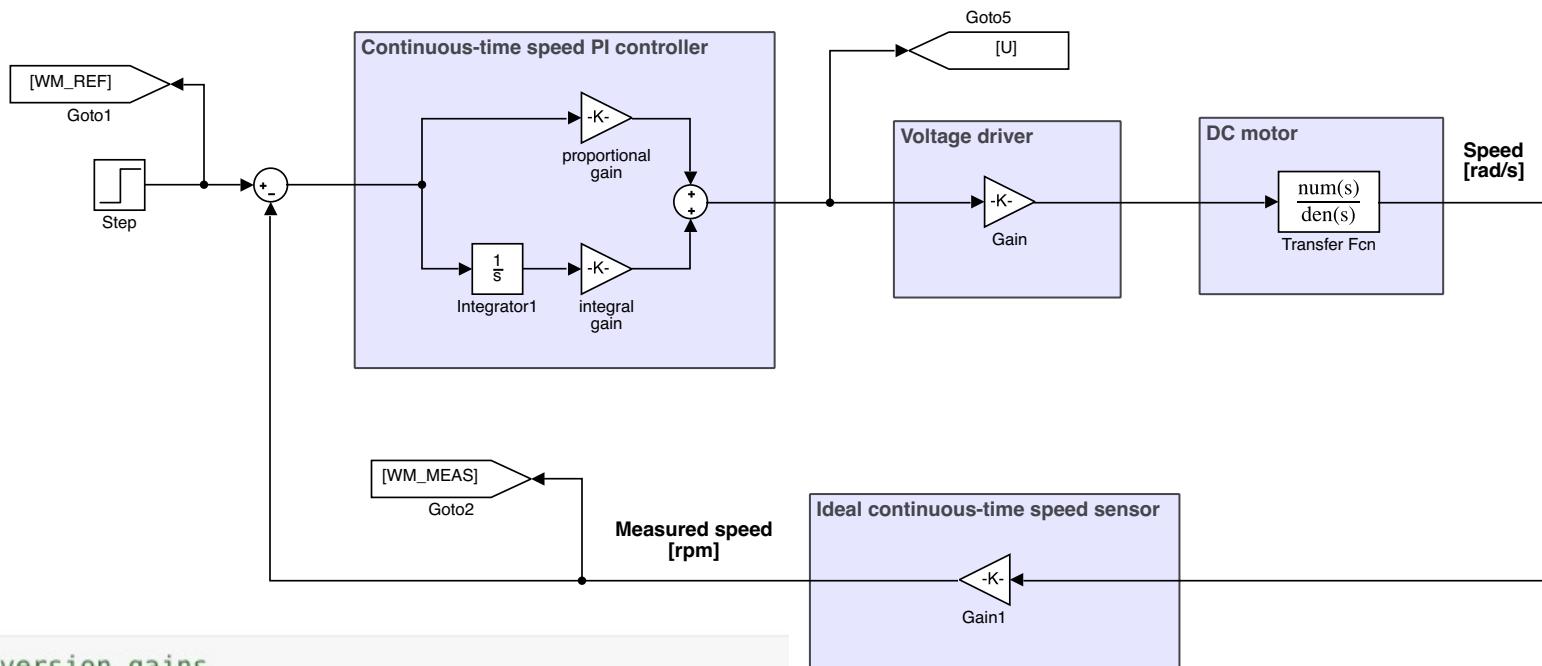
$$C(s) = \frac{U(s)}{E(s)} = K_P + \frac{K_I}{s}, \quad K_P = 8.4 \times 10^{-3} \\ K_I = 1.05$$

whose input is the speed error  $e$  [rpm], and output is the voltage command  $u$  [V] provided to the motor voltage driver.

The motor driver is modelled as a static gain:

$$\frac{U_a(s)}{U(s)} = k_{\text{drv}} = 0.6$$

# Simulation of a sampled-data system



```
% conversion gains
rads2rpm = 60/2/pi;
rpm2rads = 2*pi/60;

% DC motor data
mot.k = 8.3; % static gain
mot.T = 0.028; % dominant time constant

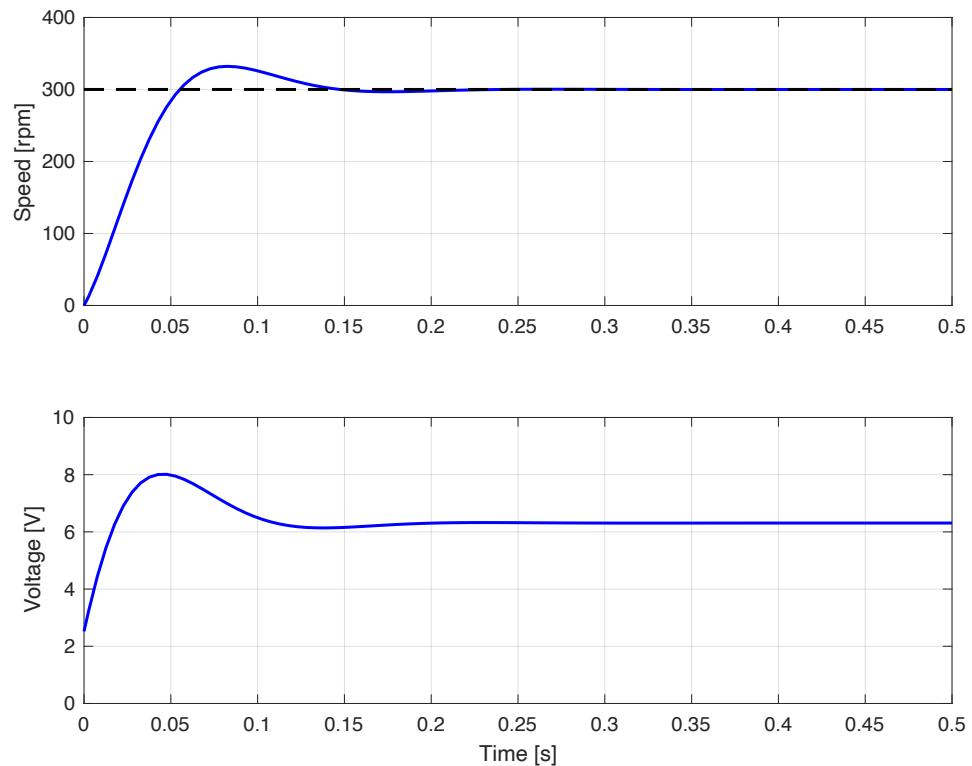
% voltage driver data
drv.kdc = 0.6; % attenuation gain

% speed PI controller data
wctrl.kp = 8.4e-3; % proportional gain
wctrl.ki = 1.05; % integral gain
```

# Simulation of a sampled-data system

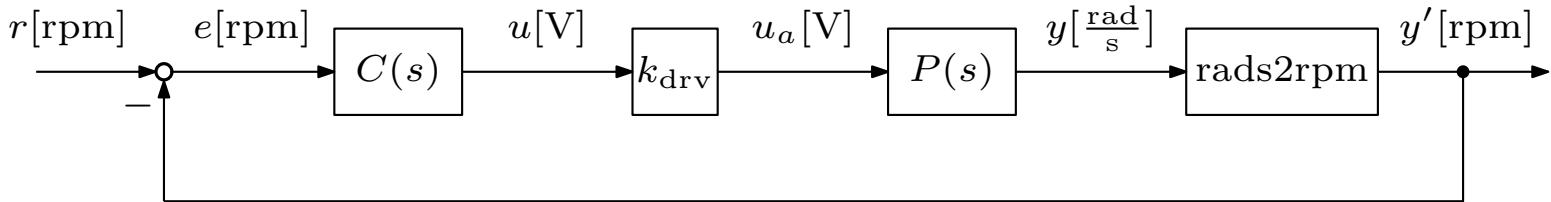
Simulation results for a step speed reference of 300 rpm, applied at  $t = 0$  s :

```
% set simulation params  
set_param('speed_ctrl_1', ...  
    'SolverType', 'Variable-step', ...  
    'Solver', 'ode45', ...  
    'MaxStep', '0.005', ...  
    'StopTime', '0.5');  
  
% run simulation  
sim('speed_ctrl_1');
```



# Simulation of a sampled-data system

Alternative: use CST (the control system is a continuous-time LTI model!).



```
% plant tf  
sysP = tf(mot.k, [mot.T, 1])
```

```
sysP =  
  
8.3  
-----  
0.028 s + 1
```

Continuous-time transfer function.

```
% controller tf  
sysC = tf([wctrl.kp, wctrl.ki], [1, 0])
```

```
sysC =  
  
0.0084 s + 1.05  
-----  
s
```

Continuous-time transfer function.

```
% closed-loop tf (from ref to out)  
sysT = feedback( sysC * drv.kdc * sysP * rads2rpm, 1 )
```

```
sysT =  
  
0.3995 s + 49.93  
-----  
0.028 s^2 + 1.399 s + 49.93
```

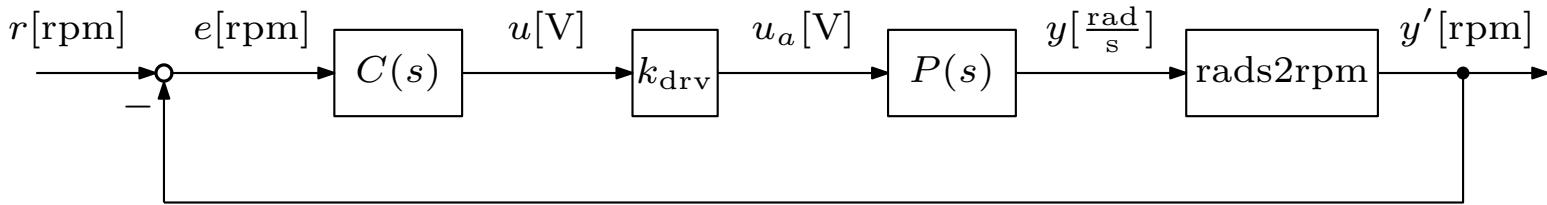
Continuous-time transfer function.

```
% closed-loop tf (from ref to controller out)  
sysCS = feedback( sysC, drv.kdc * sysP * rads2rpm )
```

```
sysCS =  
  
0.0002352 s^2 + 0.0378 s + 1.05  
-----  
0.028 s^2 + 1.399 s + 49.93
```

Continuous-time transfer function.

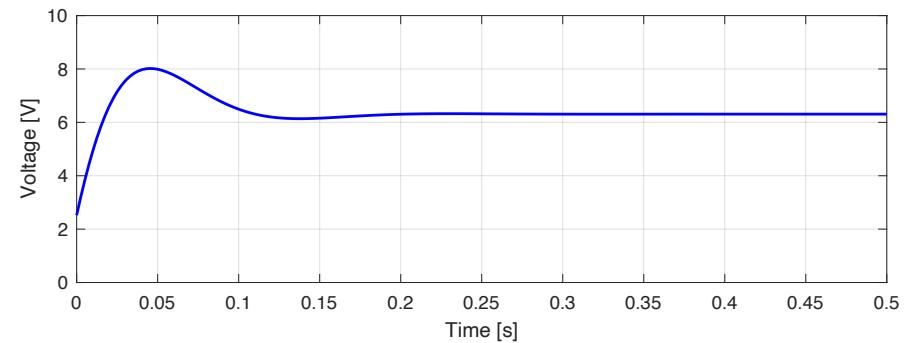
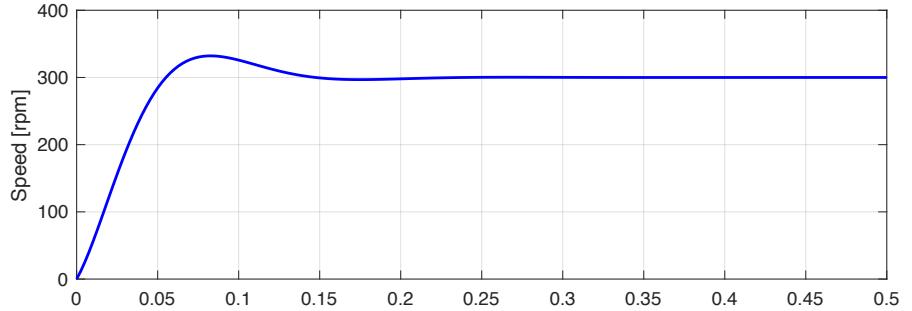
# Simulation of a sampled-data system



```
% step response
opt = stepDataOptions('InputOffset', 0, 'StepAmplitude', 300);
t = linspace(0, 0.5, 200);
y = step(sysT, t, opt);
u = step(sysCS, t, opt);

% plot results
figure;
subplot(2, 1, 1);
plot(t, y, 'b-', 'LineWidth', 1.5);
grid on;
xlim([0, t(end)]);
ylabel('Speed [rpm]');

subplot(2, 1, 2);
plot(t, u, 'b-', 'LineWidth', 1.5);
ylabel('Voltage [V]')
xlabel('Time [s]');
ylim([0, 10]);
xlim([0, t(end)]);
grid on;
```



# Simulation of a sampled-data system

Consider now the *discrete-time* PI controller:

$$K_P = 8.4 \times 10^{-3}$$

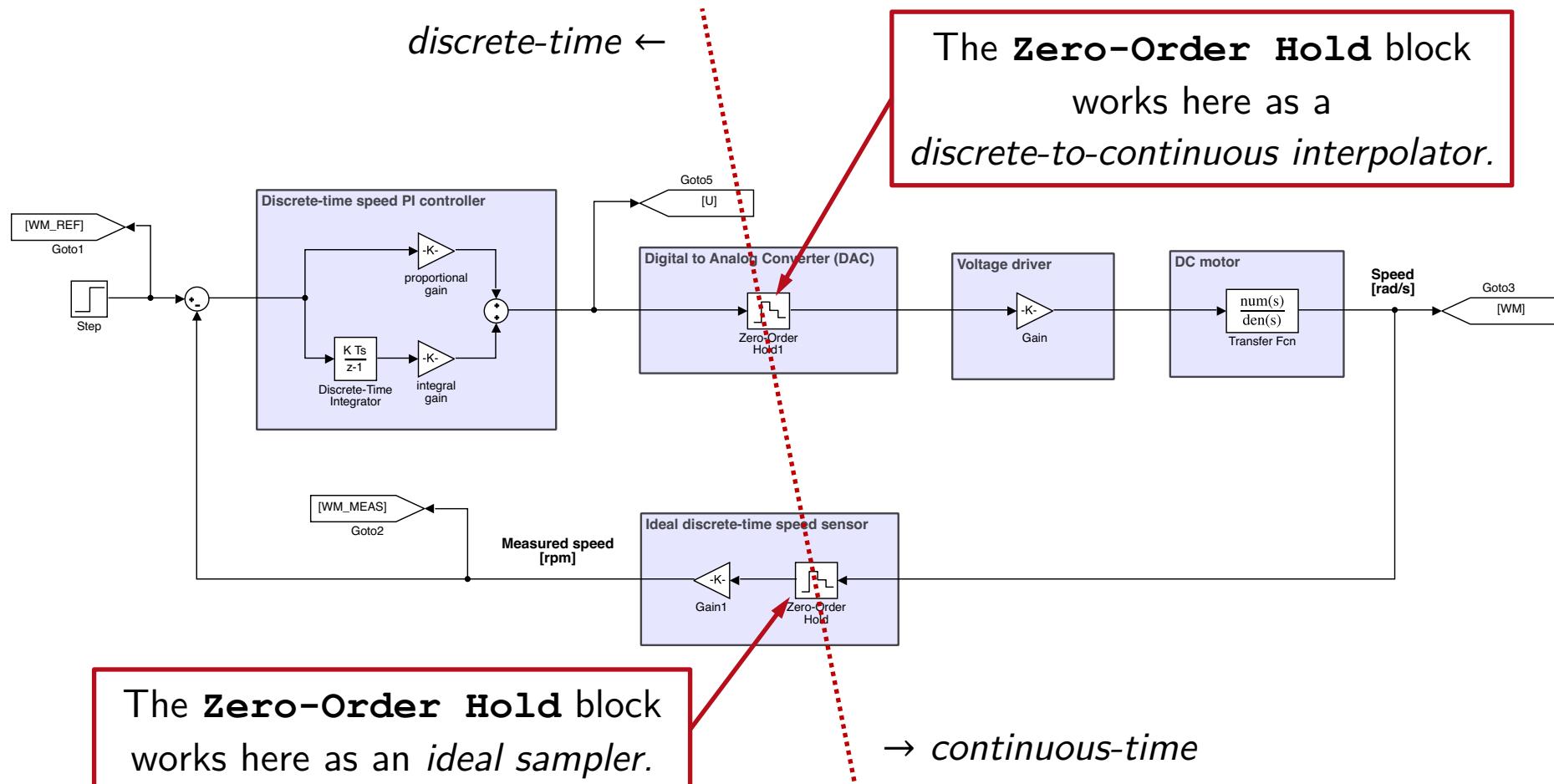
$$C(z) = \frac{U(z)}{E(z)} = K_P + \frac{K_I T_s}{z - 1}, \quad K_I = 1.05$$

$$T_s = 0.01 \text{ s}$$

obtained by discretizing the continuous-time controller with the *Forward Euler method*.

# Simulation of a sampled-data system

## Sampled-data system



# Simulation of a sampled-data system

```
% set simulation params  
set_param('speed_ctrl_2', ...  
    'SolverType', 'Variable-step', ...  
    'Solver', 'ode45', ...  
    'MaxStep', '0.001', ...  
    'StopTime', '0.5');  
  
% run simulation  
sim('speed_ctrl_2');  
  
% extract simulation results (discrete-time data)  
t = simres2.time; % time vector [s]  
wm_meas = simres2.signals(1).values(:,1); % measured motor speed [rad/s]  
wm_ref = simres2.signals(1).values(:,2); % motor speed reference [rad/s]  
u = simres2.signals(2).values(:,1); % driver command [V]  
  
% extract simulation results (continuous-time data)  
tc = simres2c.time;  
wm = simres2c.signals.values(:,1); % actual motor speed [rad/s]  
  
% plot control response  
figure;  
subplot(2, 1, 1);  
stairs(t, wm_meas, 'b-', 'LineWidth', 1.5);  
hold on;  
plot(tc, wm, 'r-', 'LineWidth', 1.5);  
stairs(t, wm_ref, 'k--', 'LineWidth', 1.5);  
grid on;  
xlim([0, 0.5]);  
ylabel('Speed [rpm]');  
legend('Actual', 'Measured');  
  
subplot(2, 1, 2);  
stairs(t, u, 'b-', 'LineWidth', 1.5);  
ylabel('Voltage [V]')  
xlabel('Time [s]');  
ylim([0, 10]);  
xlim([0, 0.5]);  
grid on;
```

Use **stairs** for drawing  
a *stair-step* plot.

