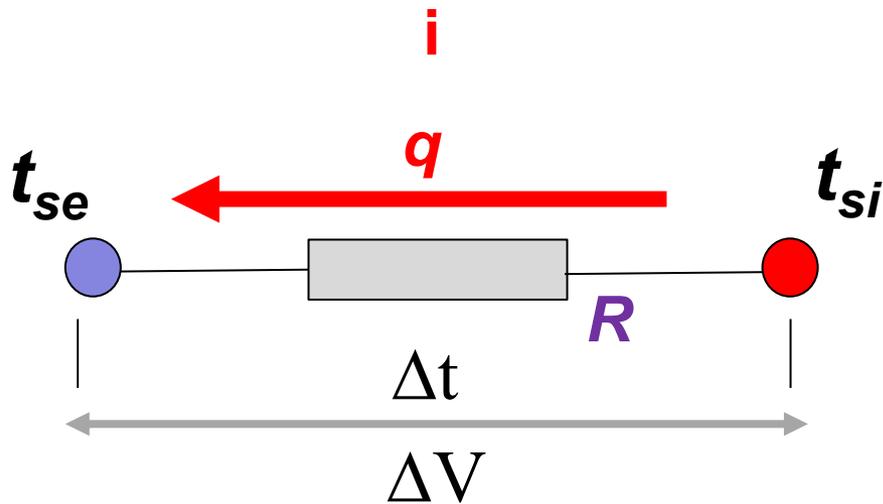


**Peak power determination,  
simplified energy demand for  
heating, schematic of heating  
systems**

# Thermal conduction

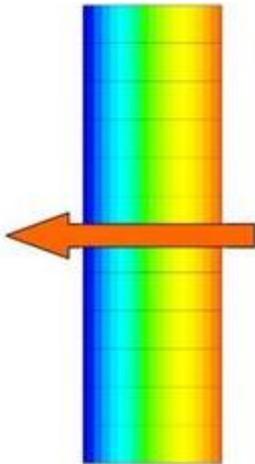
## Steady state conditions 1-D:



Single layer

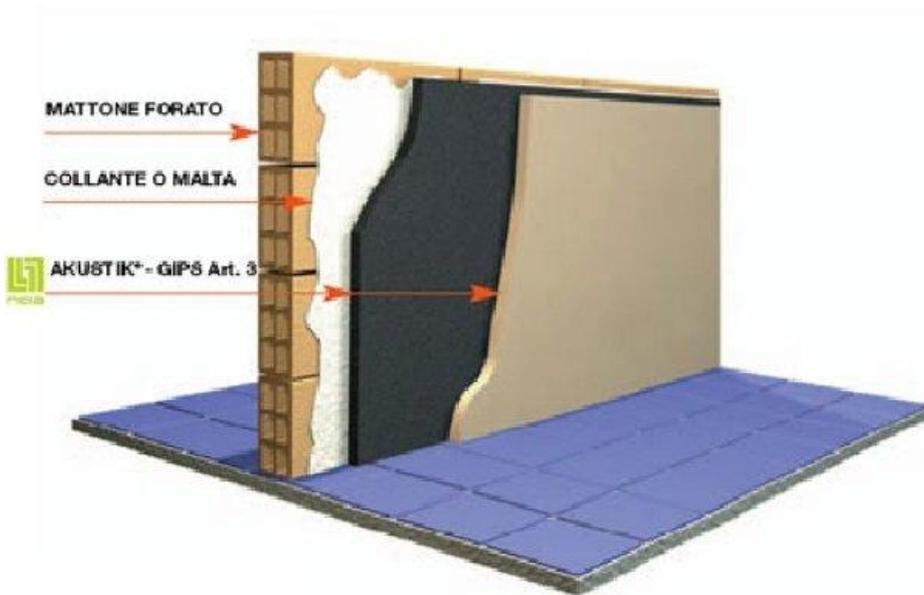
$$q = S \left( \frac{\lambda}{s} \right) (t_{si} - t_{se})$$
$$R = \frac{s}{\lambda}$$

$[m^2 K/W]$



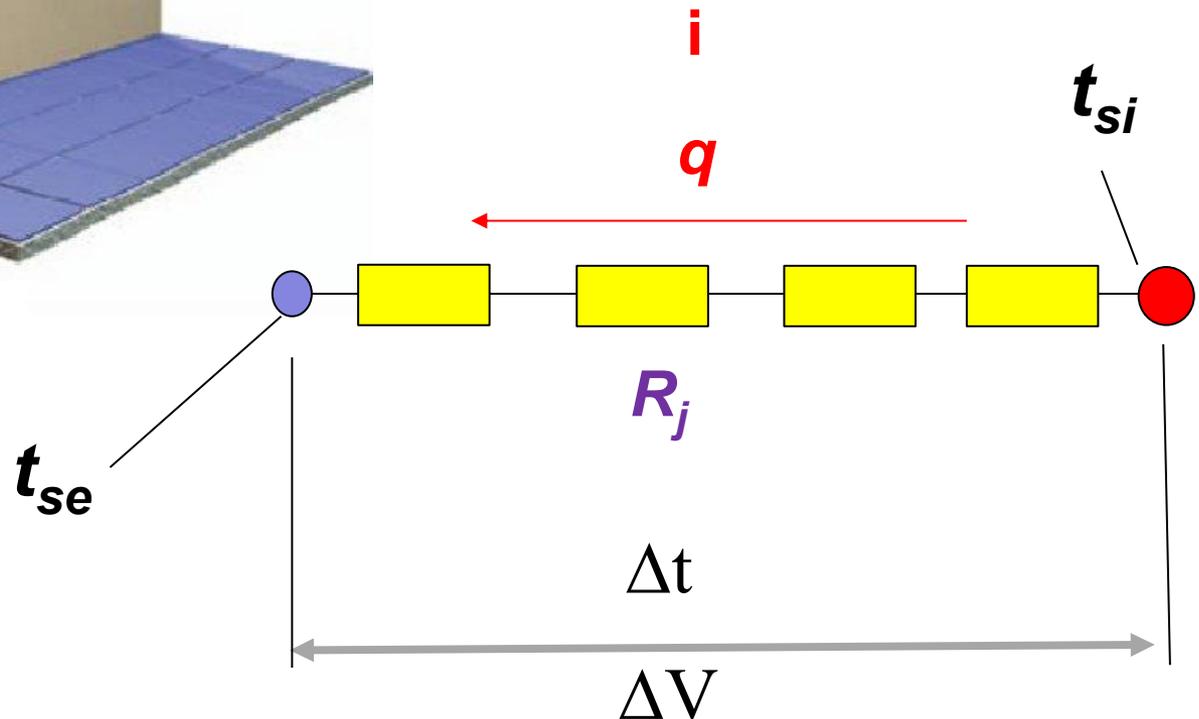
# Thermal conduction

## Steady state conditions: 1-D



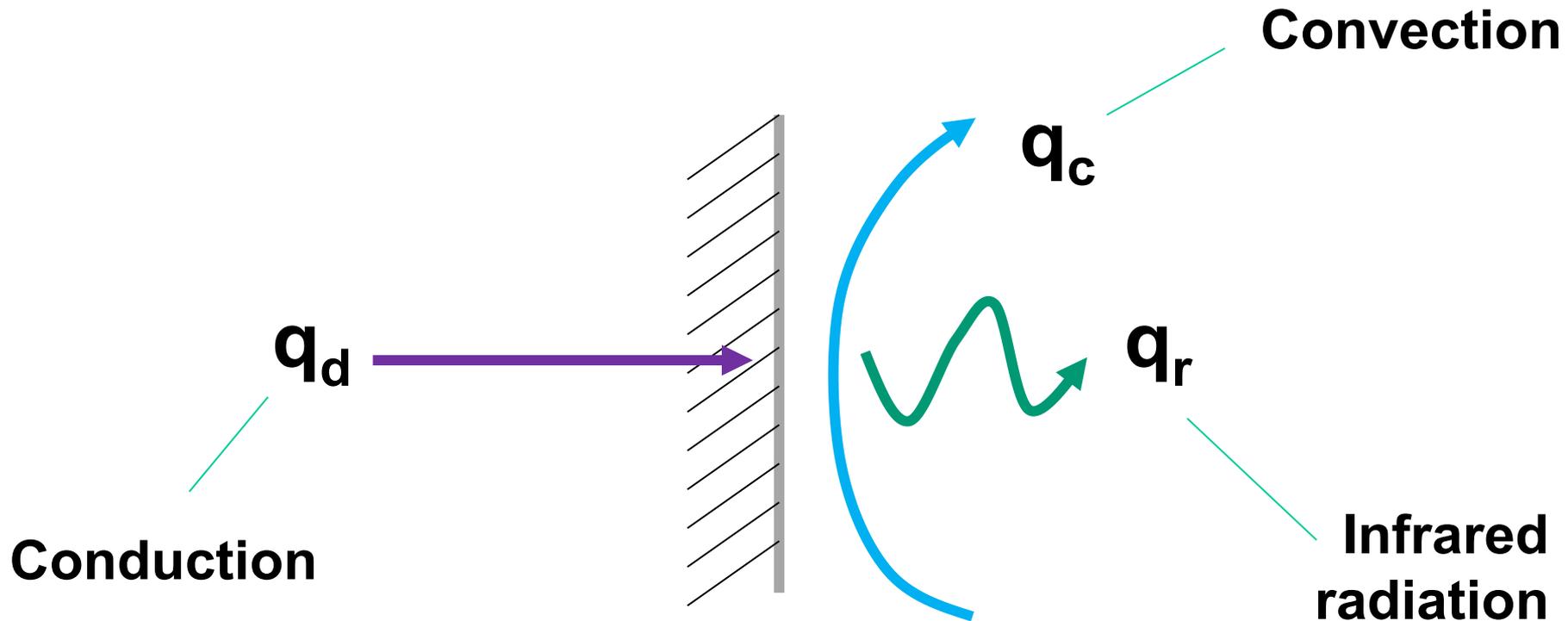
multi-layer

$$q = \frac{S (t_{si} - t_{se})}{\sum R_j}$$



# Heat transfer on surfaces

Heat balance on a surface not considering the solar gains or other radiant loads (e.g. lighting)



# Convection

A fluid flow at temperature  $t$  brushes against a solid surface at temperature  $t_s$

Heat flux:

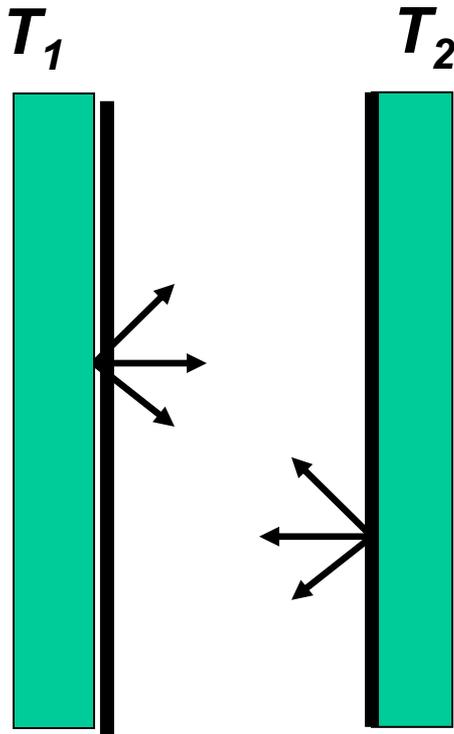
$$q = h_c S (t_s - t) \quad t_s > t$$

Coefficient of the convective heat transfer

$$h_c \text{ [W/(m}^2 \text{ K)]}$$

# Infrared radiation

Plane, parallel, front facing surfaces at temperature, respectively,  $T_1$  and  $T_2$



$$q = \frac{\sigma_n S (T_1^4 - T_2^4)}{\frac{1}{\varepsilon_1} + \frac{1}{\varepsilon_2} - 1}$$

$\sigma_n$ : Stephan-Boltzmann's constant

$5.76 \times 10^{-8} \text{ W}/(\text{m}^2 \text{ K}^4)$

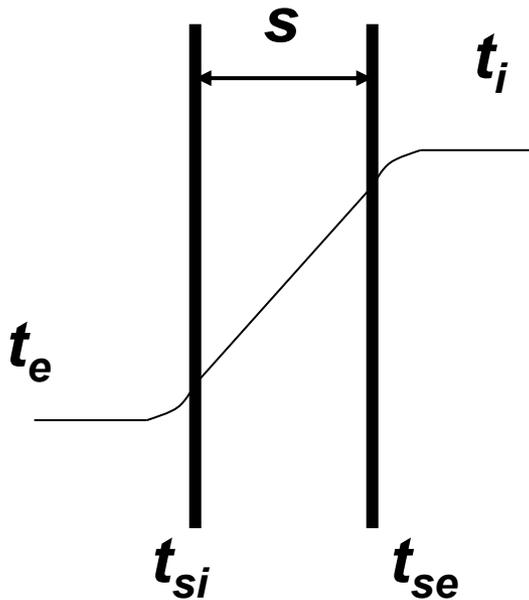
$\varepsilon_1, \varepsilon_2$ : emissivity of the two surfaces.  
For usual finishing materials of walls

$$\varepsilon_1 = \varepsilon_2 = 0.9 \quad \longrightarrow \quad 1 < \frac{1}{\varepsilon_1} + \frac{1}{\varepsilon_2} - 1 < 1.1$$

$$q = \sigma_n S (T_1^4 - T_2^4) = 4 \sigma_n S T_m^3 (T_1 - T_2) = h_r S (T_1 - T_2)$$

$h_r$  radiant heat transfer coefficient =  $5.5 \text{ W}/(\text{m}^2 \text{ K})$

# Overall heat transfer on a surface



-Outdoor temperature and indoor temperature  $t_e$  and  $t_i$

- Surface temperature  $t_{si}$   $t_{se}$

On the external surface the heat flux is:

- For convection with the external air

$$q = h_{ce} S (t_{se} - t_e)$$

- For radiation:

$$q = h_{re} S (t_{se} - t_e)$$

- overall:

$$q = (h_{re} + h_{ce}) S (t_{se} - t_e)$$

External overall heat transfer coefficient

$h_{se}$



Similarly, on the inner surface of the layer the heat flux is:

$$q = (h_{ri} + h_{ci}) S (t_{si} - t_i)$$

$h_{si}$  Internal overall heat transfer coefficient

$$h_{si} = h_{ri} + h_{ci} = 1/R_{si}$$

$$h_{se} = h_{re} + h_{ce} = 1/R_{se}$$

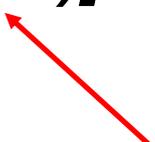
# U-value of a building element

$$q^* = \frac{\lambda}{s} (t_{si} - t_{se})$$

$$q^* = h_{si} (t_{si} - t_i)$$

$$q^* = h_{se} (t_{se} - t_e)$$

Trasmittance  
*U*-value  
[W/(m<sup>2</sup> K)]


$$U = \frac{1}{\frac{1}{h_{si}} + \sum R_j + \frac{1}{h_{se}}} = \frac{1}{R_{tot}}$$

$$R_{tot} = \frac{1}{h_{si}} + \sum R_j + \frac{1}{h_{se}}$$

$$R_{tot} = R_{si} + \sum R_j + R_{se}$$

## For a multi-layer wall:

$$U = \frac{1}{\frac{1}{h_{si}} + \sum \frac{\lambda}{s} + \sum R + \frac{1}{h_{se}}}$$

$$R_{tot} = \frac{1}{h_{si}} + \sum \frac{\lambda}{s} + \sum R + \frac{1}{h_{se}}$$

L. 10/1991

**Italian law**

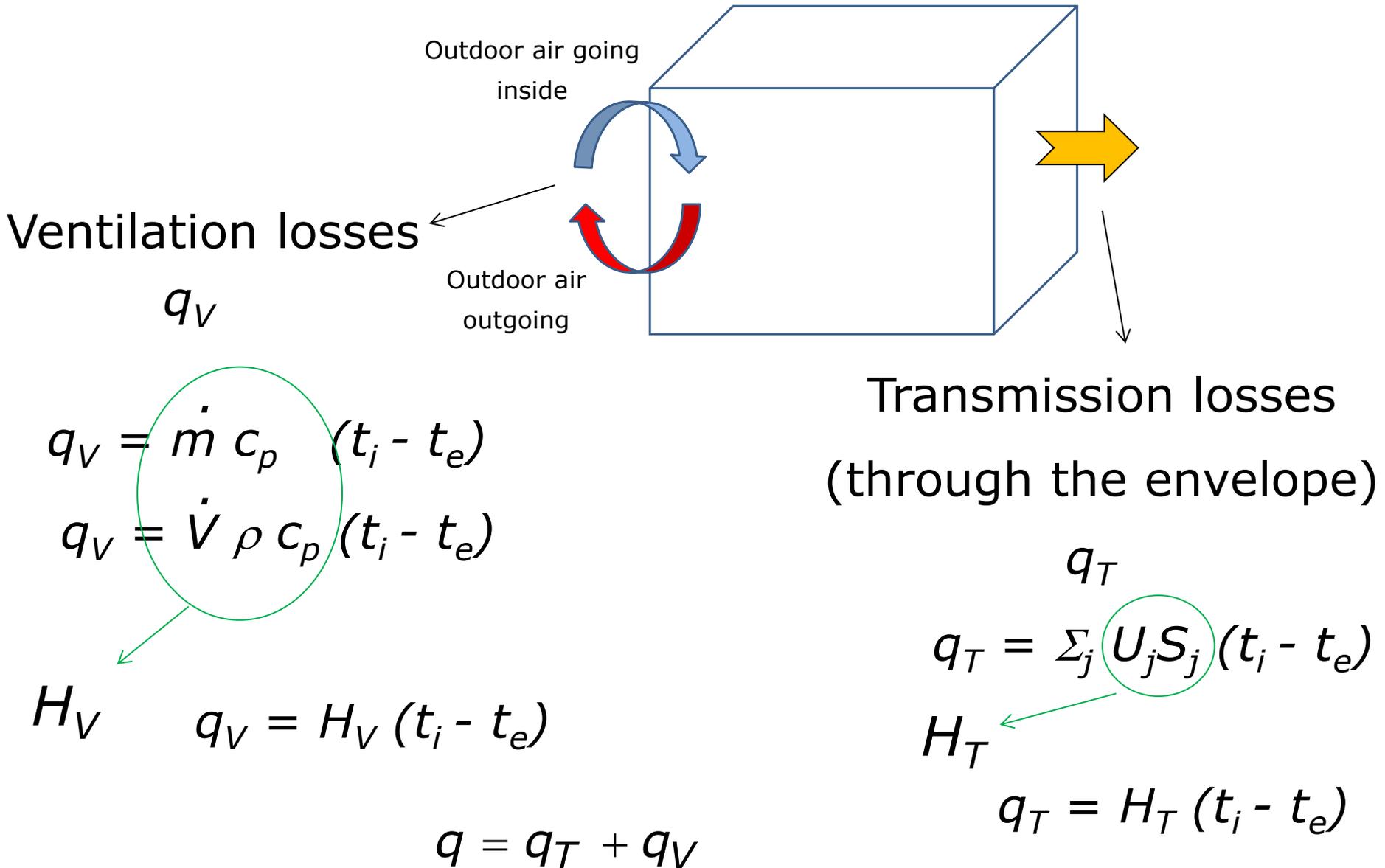
L. 373

D.Lgs. N.192

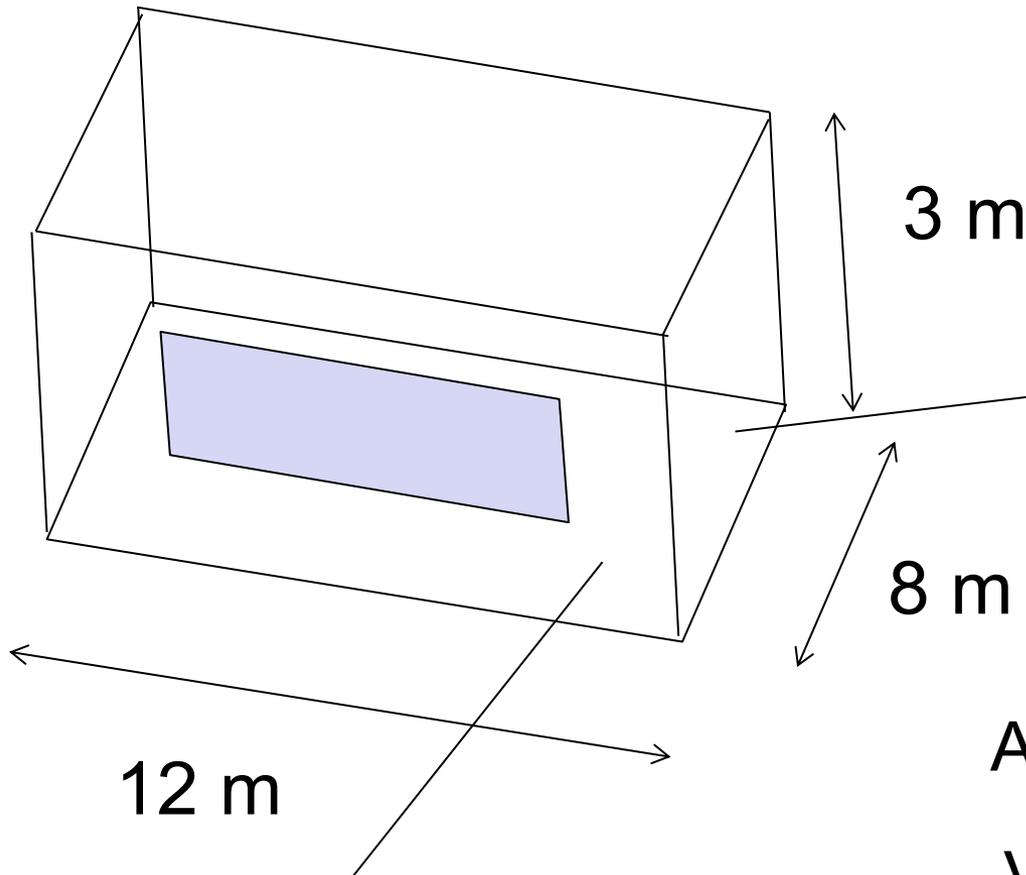
From 1/1/2021  
nZEB

	1960	1970	1976	1991	2005	Today
Walls [W/(m <sup>2</sup> K)]	1,4	1,0	0,8	0,7	0,35	0,2
Windows [W/(m <sup>2</sup> K)]	5,7	2,8	2,4	2,4	2,2	1,7
Roof [W/(m <sup>2</sup> K)]	1,0	0,8	0,6	0,5	0,33	0,2
Floor [W/(m <sup>2</sup> K)]	0,8	0,8	0,7	0,6	0,33	0,2
Specific Energy [kWh/(m <sup>2</sup> year)]	230	200	170	120	60	15

# Peak power calculation in heating



# Example



$$S_1 = 12 \times 3 = 36 \text{ m}^2$$

$$S_{\text{tot}} = 24 + 36 = 60 \text{ m}^2$$

$$A_w = 96 \times (1/6) \text{ m}^2 = 16 \text{ m}^2$$

$$S_2 = 8 \times 3 = 24 \text{ m}^2$$

$$A_f = 12 \times 8 = 96 \text{ m}^2$$

$$V = 96 \times 3 = 288 \text{ m}^3$$



$$S/V = 60/288 = 0.21 \text{ m}^{-1}$$

$$S_{\text{op}} = 60 - 16 = 44 \text{ m}^2$$

$$U_{op} = 1 \text{ W}/(\text{m}^2 \text{ K})$$

$$U_w = 6 \text{ W}/(\text{m}^2 \text{ K})$$

$$H_T = 44 \times 1 + 6 \times 16 = 140 \text{ W/K}$$

$$n = 0.5 \text{ h}^{-1}$$

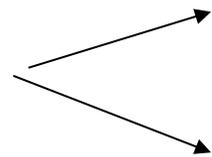
$$\dot{V} = n \times V = 0.5 \times 288 = 144 \text{ m}^3/\text{h}$$

$$H_V = \frac{\dot{V} \times \rho \times c_p}{3600} = \frac{144 \times 1.2 \times 1007}{3600} = 48 \text{ W/K}$$

$$H_{tot} = H_T + H_V = 48 + 140 = 188 \text{ W/K}$$

$$P_{tot} = 188 \times (t_i - t_e) = 188 \times 25 = 4708 \text{ W}$$

Due parametri  
Importanti:


$$P_{tot} / V = 4708/288 = 16.3 \text{ W}/\text{m}^3$$
$$P_{tot} / A_f = 4708/96 = 49 \text{ W}/\text{m}^2$$

# Case 1.a

Case 1	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	60	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.048	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	<b>1</b>	44							
Window	16	<b>6</b>	96							
Total	60		140	48	<b>3500</b>	<b>1208</b>	<b>4708</b>	<b>16.3</b>	<b>49.0</b>	
					<b>74%</b>	<b>26%</b>				

# Case 2.a

Case 2	<b>2 surfaces + roof</b>									
Length	12 m									
Width	8 m									
Height	3 m		cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5 1/h</b>				[°C]	[°C]	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	156	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.048	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	<b>1</b>	140							
Window	16	<b>6</b>	96							
Total	156		236	48	<b>5900</b>	<b>1208</b>	<b>7108</b>	<b>24.7</b>	<b>74.0</b>	
					<b>83%</b>	<b>17%</b>				

# Case 3.a

Case 3	2 surfaces									
Length	12 m									
Width	8 m									
Height	3 m		cp	1007	J/(kg K)			ti	te	Dt
Af	96	m <sup>2</sup>	n	1	1/h			[°C]	[°C]	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			20	-5	25
Stot	60	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.096	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	97	3500	2417	5917	20.5	61.6	
					59%	41%				

# Case 4.a

<b>Case 4</b>	<b>2 surfaces + roof</b>									
Length	12 m									
Width	8 m									
Height	3 m		cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	156	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.096	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	<b>1</b>	140							
Window	16	<b>6</b>	96							
Total	156		236	97	<b>5900</b>	<b>2417</b>	<b>8317</b>	<b>28.9</b>	<b>86.6</b>	
					<b>71%</b>	<b>29%</b>				

## Summary of cases «a»:

- Outdoor temperature  $-5^{\circ}\text{C}$
- High U-values

- Case 1.a:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
3.5	1.2	4.7	16	49
74%	26%			

- Case 2.a:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
5.9	1.2	7.1	25	74
85%	15%			

- Case 3.a:**
- 2 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
3.5	2.4	5.9	20	62
60%	40%			

- Case 4.a:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
5.9	2.4	8.3	29	87
70%	30%			

# Case 1.b

Case 1.b	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			[°C]	[°C]	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	60	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.048	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	48	<b>4900</b>	<b>1692</b>	<b>6592</b>	<b>22.9</b>	<b>68.7</b>	
					<b>74%</b>	<b>26%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	48	<b>3500</b>	<b>1208</b>	<b>4708</b>	<b>16.3</b>	<b>49.0</b>	
					<b>74%</b>	<b>26%</b>				

# Case 2.b

<b>Case 2.b</b>	<b>2 surfaces + roof</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	156	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.048	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	48	<b>8260</b>	<b>1692</b>	<b>9952</b>	<b>34.6</b>	<b>103.7</b>	
					<b>83%</b>	<b>17%</b>				
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	48	<b>5900</b>	<b>1208</b>	<b>7108</b>	<b>24.7</b>	<b>74.0</b>	
					<b>83%</b>	<b>17%</b>				

# Case 3.b

<b>Case 3.b</b>	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)					
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>					
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h					
Stot	60	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.096	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	<b>1</b>	44							
Window	16	<b>6</b>	96							
Total	60		140	97	<b>4900</b>	<b>3384</b>	<b>8284</b>	<b>28.8</b>	<b>86.3</b>	
					<b>59%</b>	<b>41%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	97	<b>3500</b>	<b>2417</b>	<b>5917</b>	<b>20.5</b>	<b>61.6</b>	
					<b>59%</b>	<b>41%</b>				

# Case 4.b

Case 4.b	<b>2 surfaces + roof</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	156	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.096	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	97	<b>8260</b>	<b>3384</b>	<b>11644</b>	<b>40.4</b>	<b>121.3</b>	
					<b>71%</b>	<b>29%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	97	<b>5900</b>	<b>2417</b>	<b>8317</b>	<b>28.9</b>	<b>86.6</b>	
					<b>71%</b>	<b>29%</b>				

## Summary of cases «b»:

- Outdoor temperature  $-15^{\circ}\text{C}$
- High U-values

- Case 1.b:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
4.9	1.7	6.6	23	69
75%	25%			

- Case 2.b:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
8.3	1.7	10.0	35	105
85%	15%			

- Case 3.b:**
- 2 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
4.9	3.4	8.3	29	87
60%	40%			

- Case 4.b:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
8.3	3.4	11.7	40	121
70%	30%			

# Case 1.c

Case 1.c	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			[°C]	[°C]	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	60	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.048	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	<b>0.2</b>	8.8							
Window	16	<b>2</b>	32							
Total	60		40.8	48	<b>1020</b>	<b>1208</b>	<b>2228</b>	<b>7.7</b>	<b>23.2</b>	
					<b>46%</b>	<b>54%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	48	<b>3500</b>	<b>1208</b>	<b>4708</b>	<b>16.3</b>	<b>49.0</b>	
					<b>74%</b>	<b>26%</b>				

# Case 2.c

Case 2.c	2 surfaces + roof									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			ti	te	Dt
Af	96	m <sup>2</sup>	n	0.5	1/h			[°C]	[°C]	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			20	-5	25
Stot	156	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.048	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	0.2	28							
Window	16	2	32							
Total	156		60	48	1500	1208	2708	9.4	28.2	
					55%	45%				
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	48	5900	1208	7108	24.7	74.0	
					83%	17%				

# Case 3.c

Case 3.c	<b>2 surfaces</b>									
Length	12 m									
Width	8 m									
Height	3 m		cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	60	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.096	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	0.2	8.8							
Window	16	2	32							
Total	60		40.8	97	<b>1020</b>	<b>2417</b>	<b>3437</b>	<b>11.9</b>	<b>35.8</b>	
					<b>30%</b>	<b>70%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	97	<b>3500</b>	<b>2417</b>	<b>5917</b>	<b>20.5</b>	<b>61.6</b>	
					<b>59%</b>	<b>41%</b>				

# Case 4.c

Case 4.c	<b>2 surfaces + roof</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			ti	te	Dt
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			[°C]	[°C]	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-5</b>	<b>25</b>
Stot	156	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.096	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	0.2	28							
Window	16	2	32							
Total	156		60	97	<b>1500</b>	<b>2417</b>	<b>3917</b>	<b>13.6</b>	<b>40.8</b>	
					<b>38%</b>	<b>62%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	97	<b>5900</b>	<b>2417</b>	<b>8317</b>	<b>28.9</b>	<b>86.6</b>	
					<b>71%</b>	<b>29%</b>				

## Summary of cases «c»:

- Outdoor temperature  $-5^{\circ}\text{C}$
- Low U-values

- Case 1.c:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.0	1.2	2.2	8	23
45%	55%			

- Case 2.c:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.5	1.2	2.7	10	28
55%	45%			

- Case 3.c:**
- 2 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.0	2.4	3.4	12	36
30%	70%			

- Case 4.c:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.5	2.4	3.9	14	41
40%	60%			

# Case 1.d

Case 1.d	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			[°C]	[°C]	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	60	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.048	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	<b>0.15</b>	6.6							
Window	16	<b>1.5</b>	24							
Total	60		30.6	48	<b>1071</b>	<b>1692</b>	<b>2763</b>	<b>9.6</b>	<b>28.8</b>	
					<b>39%</b>	<b>61%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	48	<b>4900</b>	<b>1692</b>	<b>6592</b>	<b>22.9</b>	<b>68.7</b>	
					<b>74%</b>	<b>26%</b>				

# Case 2.d

Case 2.d	<b>2 surfaces + roof</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>0.5</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		144	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	156	m <sup>2</sup>	m	172.8	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.048	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	0.15	21							
Window	16	1.5	24							
Total	156		45	48	<b>1575</b>	<b>1692</b>	<b>3267</b>	<b>11.3</b>	<b>34.0</b>	
					<b>48%</b>	<b>52%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	48	<b>8260</b>	<b>1692</b>	<b>9952</b>	<b>34.6</b>	<b>103.7</b>	
					<b>83%</b>	<b>17%</b>				

# Case 3.d

Case 3.d	<b>2 surfaces</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	60	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.208333	m <sup>-1</sup>		0.096	kg/s					
	S	<b>U</b>	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	<b>[W/(m<sup>2</sup> K)]</b>	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	0.15	6.6							
Window	16	1.5	24							
Total	60		30.6	97	<b>1071</b>	<b>3384</b>	<b>4455</b>	<b>15.5</b>	<b>46.4</b>	
					<b>24%</b>	<b>76%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	44	1	44							
Window	16	6	96							
Total	60		140	97	<b>4900</b>	<b>3384</b>	<b>8284</b>	<b>28.8</b>	<b>86.3</b>	
					<b>59%</b>	<b>41%</b>				

# Case 4.d

Case 4.d	<b>2 surfaces + roof</b>									
Length	12	m								
Width	8	m								
Height	3	m	cp	1007	J/(kg K)			<b>ti</b>	<b>te</b>	<b>Dt</b>
Af	96	m <sup>2</sup>	<b>n</b>	<b>1</b>	<b>1/h</b>			<b>[°C]</b>	<b>[°C]</b>	
V	288	m <sup>3</sup>		288	m <sup>3</sup> /h			<b>20</b>	<b>-15</b>	<b>35</b>
Stot	156	m <sup>2</sup>	m	345.6	kg/h					
Stot/V	0.541667	m <sup>-1</sup>		0.096	kg/s					
	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	0.15	21							
Window	16	1.5	24							
Total	156		45	97	<b>1575</b>	<b>3384</b>	<b>4959</b>	<b>17.2</b>	<b>51.7</b>	
					<b>32%</b>	<b>68%</b>				

	S	U	HT	HV	PT	PV	Ptot	PV	PS	
	[m <sup>2</sup> ]	[W/(m <sup>2</sup> K)]	[W/K]	[W/K]	[W]	[W]	[W]	[W/m <sup>3</sup> ]	[W/m <sup>2</sup> ]	
Opaque	140	1	140							
Window	16	6	96							
Total	156		236	97	<b>8260</b>	<b>3384</b>	<b>11644</b>	<b>40.4</b>	<b>121.3</b>	
					<b>71%</b>	<b>29%</b>				

# Summary of cases «d»:

- Outdoor temperature  $-15^{\circ}\text{C}$
- Low U-values

- Case 1.d:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.1	1.7	2.8	10	30
40%	60%			

- Case 2.d:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.6	1.7	3.3	12	35
50%	50%			

- Case 3.d:**
- 2 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.1	3.4	4.5	16	47
25%	75%			

- Case 4.d:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.6	3.4	5.0	18	52
30%	70%			

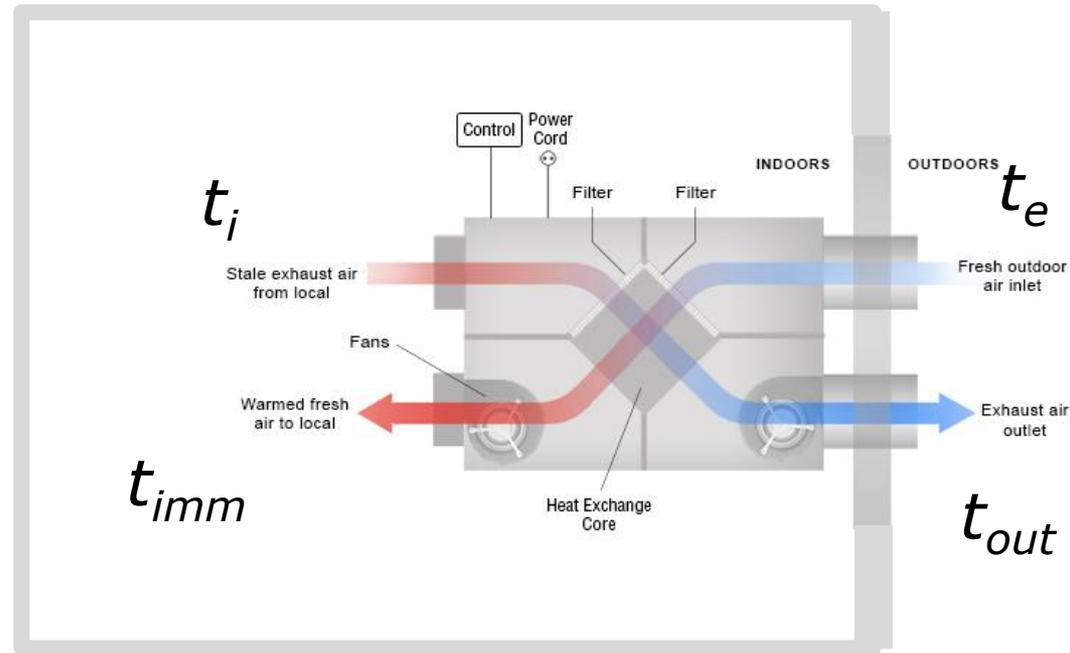
# Heat recovery on ventilation

Overall heat loss:

$$q_V = \dot{m} c_p (t_i - t_e)$$

$$\varepsilon = \frac{\text{Heat recovery}}{\text{Overall heat loss}}$$

$$\varepsilon = \frac{\dot{m} c_p (t_{imm} - t_e)}{\dot{m} c_p (t_i - t_e)}$$

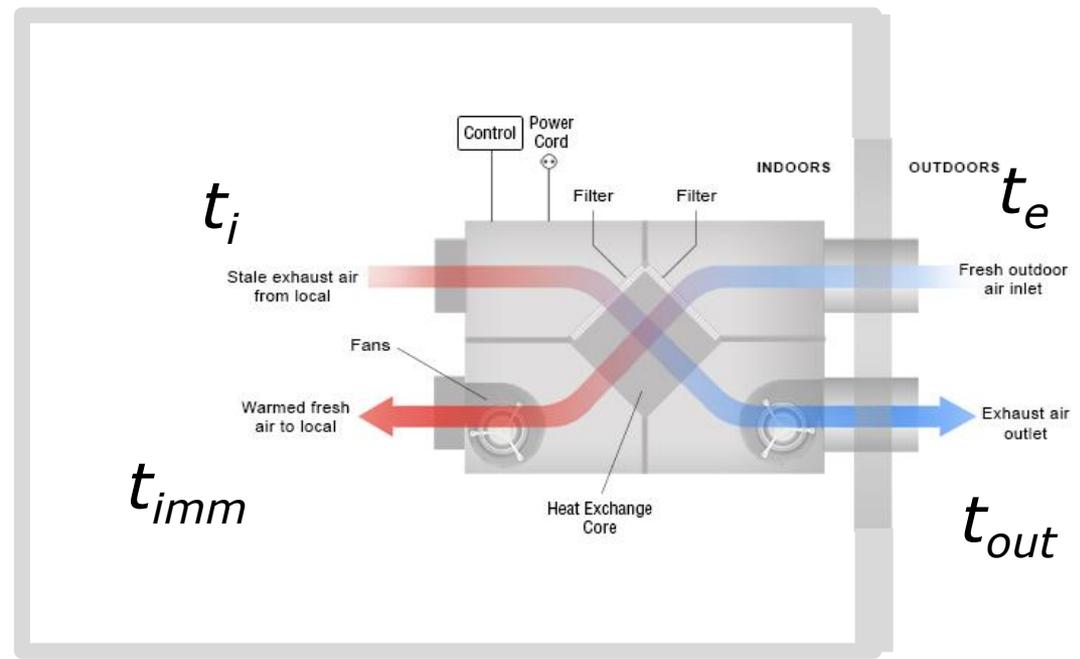


$$\varepsilon = \frac{(t_{imm} - t_e)}{(t_i - t_e)}$$

Ventilation loss:

$$q_V = \dot{m} c_p (t_i - t_{imm})$$

$$\varepsilon = \frac{(t_{imm} - t_e)}{(t_i - t_e)}$$



$$\varepsilon = \frac{(-t_i + t_{imm} + t_i - t_e)}{(t_i - t_e)} = \frac{(t_{imm} - t_i) + (t_i - t_e)}{(t_i - t_e)} = \frac{(t_{imm} - t_i)}{(t_i - t_e)} + 1$$

$$(t_i - t_{imm}) = (1 - \varepsilon) (t_i - t_e)$$

$$q_V = \dot{m} c_p (t_i - t_{imm}) = \dot{m} c_p (1 - \varepsilon) (t_i - t_e)$$

$H_V$

**Cases 1 - 2: n = 0.5 Vol./h**

$$H_V = n \dot{V} \rho c_p / 3600 = 48 \text{ W/K}$$

**Cases 3 - 4: n = 1.0 Vol./h**

$$H_V = n \dot{V} \rho c_p / 3600 = 96 \text{ W/K}$$

**Heat recovery ( $\varepsilon = 75\%$ ):**

**Cases 1.e – 2.e – 1.f – 2.f:**

**n = 0.5 Vol./h**

$$H_V = (1-\varepsilon) n \dot{V} \rho c_p / 3600 = 12 \text{ W/K}$$

**Cases 3.e – 4.e – 3.f – 4.f:**

**n = 1.0 Vol./h**

$$H_V = (1-\varepsilon) n \dot{V} \rho c_p / 3600 = 24 \text{ W/K}$$

## Summary of cases «e»:

- Outdoor temperature  $-5^{\circ}\text{C}$
- Low U-values, heat recovery unit ( $\varepsilon = 75\%$ )

- Case 1.e:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.0	0.3	1.3	5	14
75%	25%			

- Case 2.e:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.5	0.3	1.8	7	19
85%	15%			

- Case 3.e:**
- 2 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.0	0.6	1.6	6	17
65%	35%			

- Case 4.e:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.5	0.6	2.1	8	22
70%	30%			

## Summary of cases «f»:

- Outdoor temperature  $-15^{\circ}\text{C}$
- Low U-values, heat recovery unit ( $\varepsilon = 75\%$ )

- Case 1.f:**
- 2 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.1	0.4	1.5	6	16
70%	30%			

- Case 2.f:**
- 3 surfaces
  - $n = 0.5$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.6	0.4	2.0	7	21
80%	20%			

- Case 3.f:**
- 2 surfaces
  - $n = 1.0$  ACH

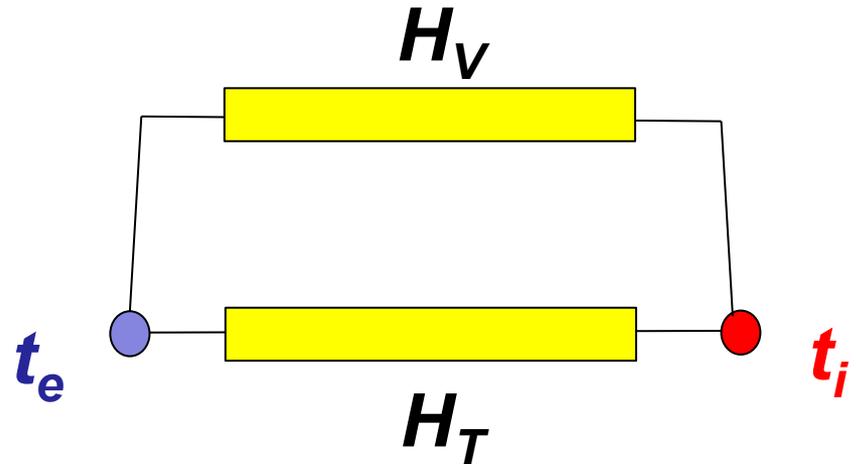
PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.1	0.8	1.9	7	20
55%	45%			

- Case 4.f:**
- 3 surfaces
  - $n = 1.0$  ACH

PT [kW]	PV [kW]	Ptot [kW]	PV [W/m <sup>3</sup> ]	PS [W/m <sup>2</sup> ]
1.6	0.8	2.4	9	26
65%	35%			

# Energy demand with a simplified method

Steady state model can be used for determining the energy demand of the building, due to the use of the temperature difference between inside and outside.



In a simplified way, it is possible to assume that the energy demand is related to Degree Days (DD), or to average monthly temperature:

$$Q_{heating} = DD \cdot (H_T + H_V) \cdot 24 / 1000$$

Very rough estimation of the heating energy demand [kWh].

Main simplifications: no effects of solar radiation and/or internal gains, no building capacitance

# **Simplified energy demand in the examples**

**Usually the energy demand of buildings is referred to the floor area ( $A_f$ ). This way it is possible to compare different buildings.**

**The following hypotheses have been chosen:**

**For the climate with  $t_e = -5^\circ\text{C}$  we consider 2500 DD**

**For the climate with  $t_e = -15^\circ\text{C}$  we consider 4000 DD**

**For costs we consider 0.08 €/kWh of thermal energy**

# Simplified energy demand in the examples

	<b>Case 1.a</b>	<b>Case 2.a</b>	<b>Case 3.a</b>	<b>Case 4.a</b>
<b>Htot</b>	188	284	237	333
<b>Energy [MWh]</b>	11.3	17.1	14.2	20.0
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	118	178	148	208
<b>Cost [€]</b>	904 €	1,365 €	1,136 €	1,597 €

	<b>Case 1.b</b>	<b>Case 2.b</b>	<b>Case 3.b</b>	<b>Case 4.b</b>
<b>Htot</b>	188	284	237	333
<b>Energy [MWh]</b>	18.1	27.3	22.7	31.9
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	188	284	237	333
<b>Cost [€]</b>	1,446 €	2,184 €	1,818 €	2,555 €

	<b>Case 1.c</b>	<b>Case 2.c</b>	<b>Case 3.c</b>	<b>Case 4.c</b>
<b>Htot</b>	89	108	137	157
<b>Energy [MWh]</b>	5.3	6.5	8.2	9.4
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	56	68	86	98
<b>Cost [€]</b>	428 €	520 €	660 €	752 €

	<b>Case 1.d</b>	<b>Case 2.d</b>	<b>Case 3.d</b>	<b>Case 4.d</b>
<b>Htot</b>	79	93	127	142
<b>Energy [MWh]</b>	7.6	9.0	12.2	13.6
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	79	93	127	142
<b>Cost [€]</b>	606 €	717 €	977 €	1,088 €

	<b>Case 1.e</b>	<b>Case 2.e</b>	<b>Case 3.e</b>	<b>Case 4.e</b>
<b>Htot</b>	53	72	65	84
<b>Energy [MWh]</b>	3.2	4.3	3.9	5.1
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	33	45	41	53
<b>Cost [€]</b>	254 €	346 €	312 €	404 €

	<b>Case 1.f</b>	<b>Case 2.f</b>	<b>Case 3.f</b>	<b>Case 4.f</b>
<b>Htot</b>	43	57	55	69
<b>Energy [MWh]</b>	4.1	5.5	5.3	6.6
<b>Specific energy [kWh/(m<sup>2</sup> year)]</b>	43	57	55	69
<b>Cost [€]</b>	328 €	438 €	421 €	531 €

# Lessons learnt from the examples

The peak load depends on:

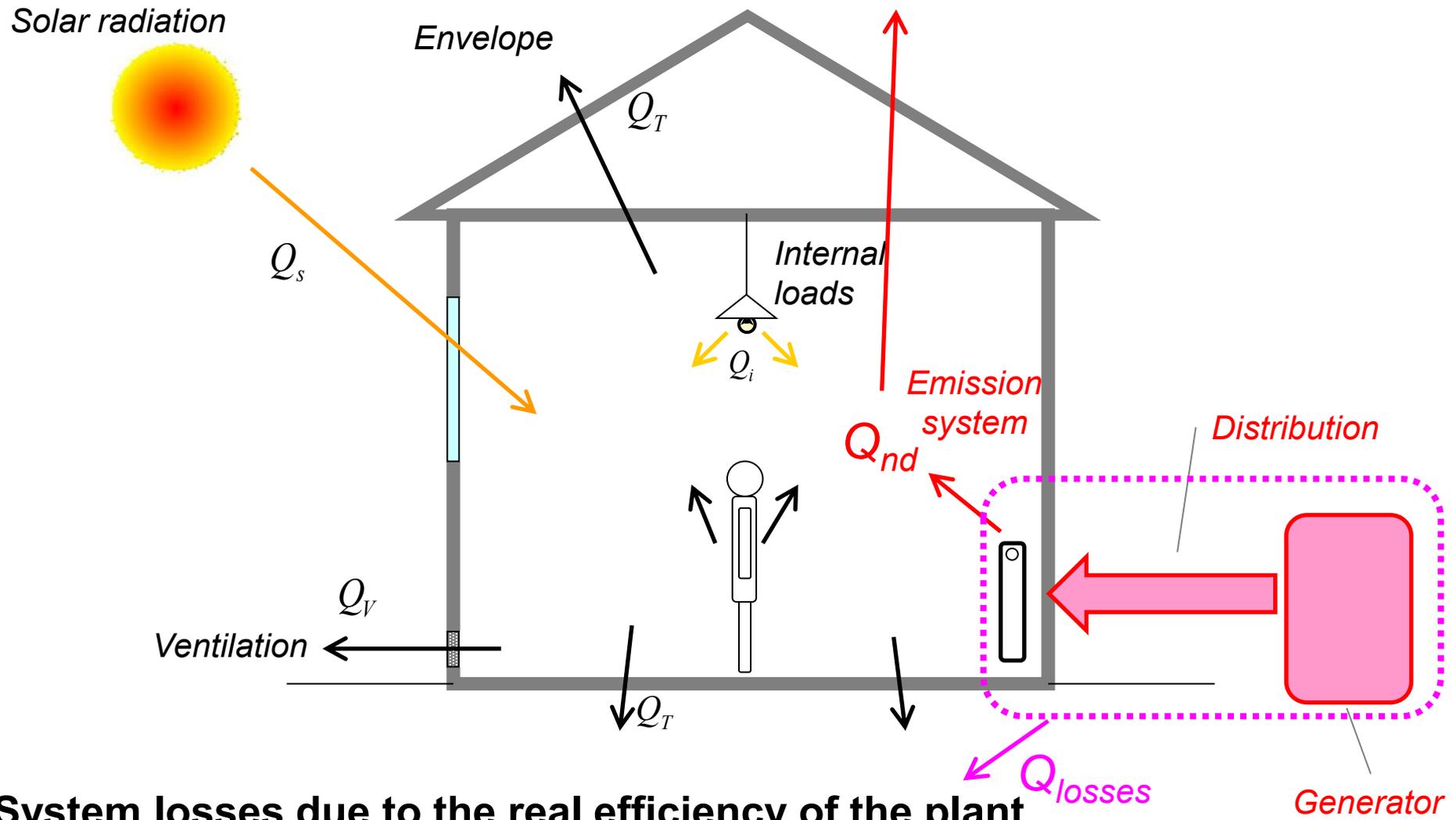
- the level of insulation (U-value)
- the amount of ventilation (flow rate)
- the climate
- the presence of a heat recovery unit

The energy demand depends on the same parameters.

The energy demand for residential buildings is expressed as kWh/(m<sup>2</sup> year)

# How can we define the energy levels?

Ideal energy required by the plant to keep an indoor temperature over the season. The plant is considered to have 100% efficiency



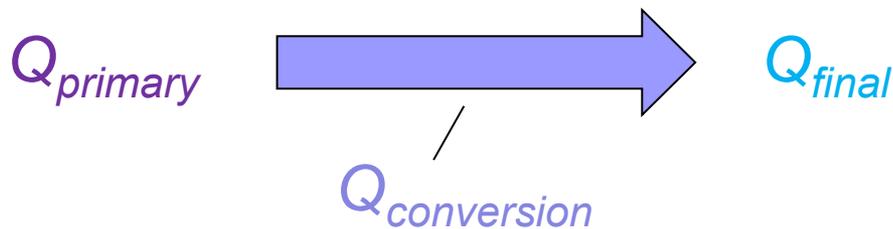
**System losses due to the real efficiency of the plant (emission system, distribution system, generator)**

**Final energy, energy consumption, on-site energy: net energy demand added the losses of the system**

**Net energy demand + losses of the system =** **Final energy, Energy consumption, Site energy, Energy use**

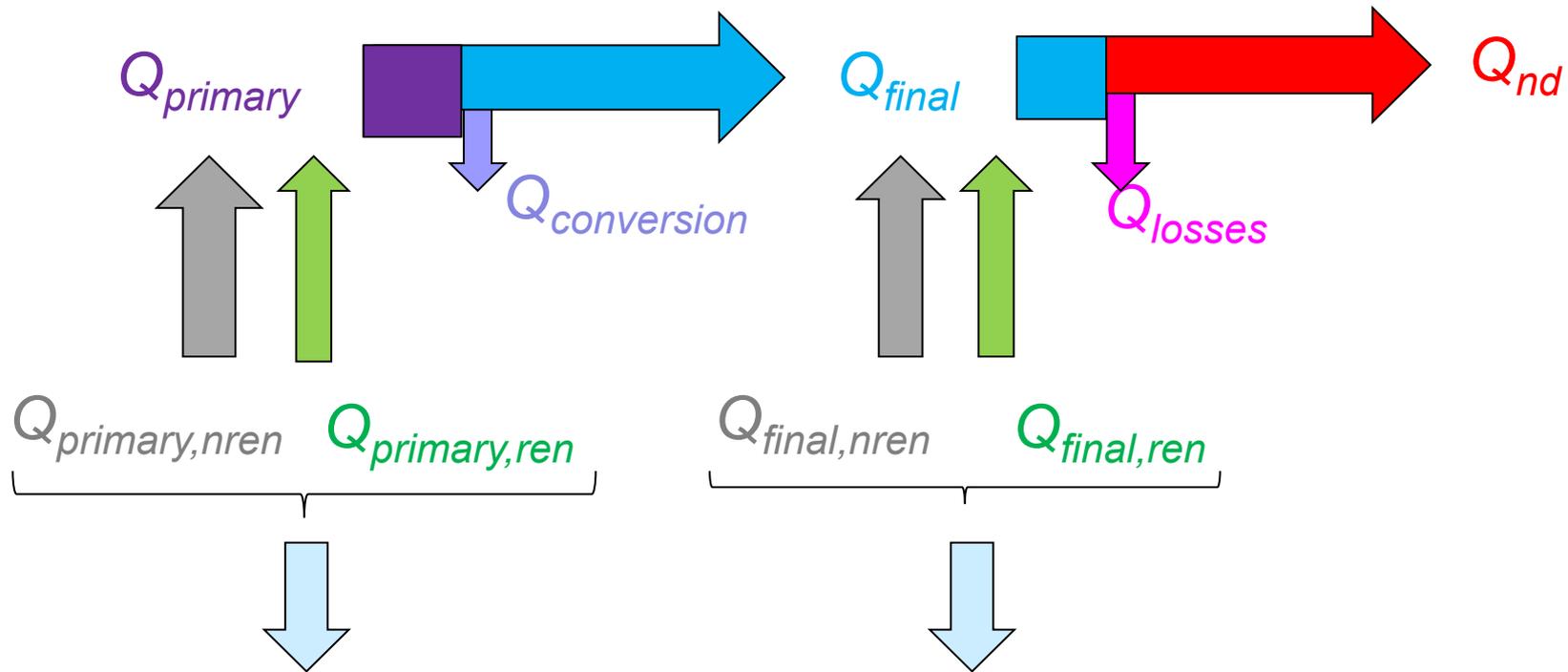
$$Q_{final} = Q_{nd} + Q_{losses}$$

**The cost we have evaluated does not take into account the efficiency of the system and hence its losses.**



**Final energy + conversion losses =** **Primary energy Source energy**

$$Q_{primary} = Q_{final} + Q_{conversion}$$

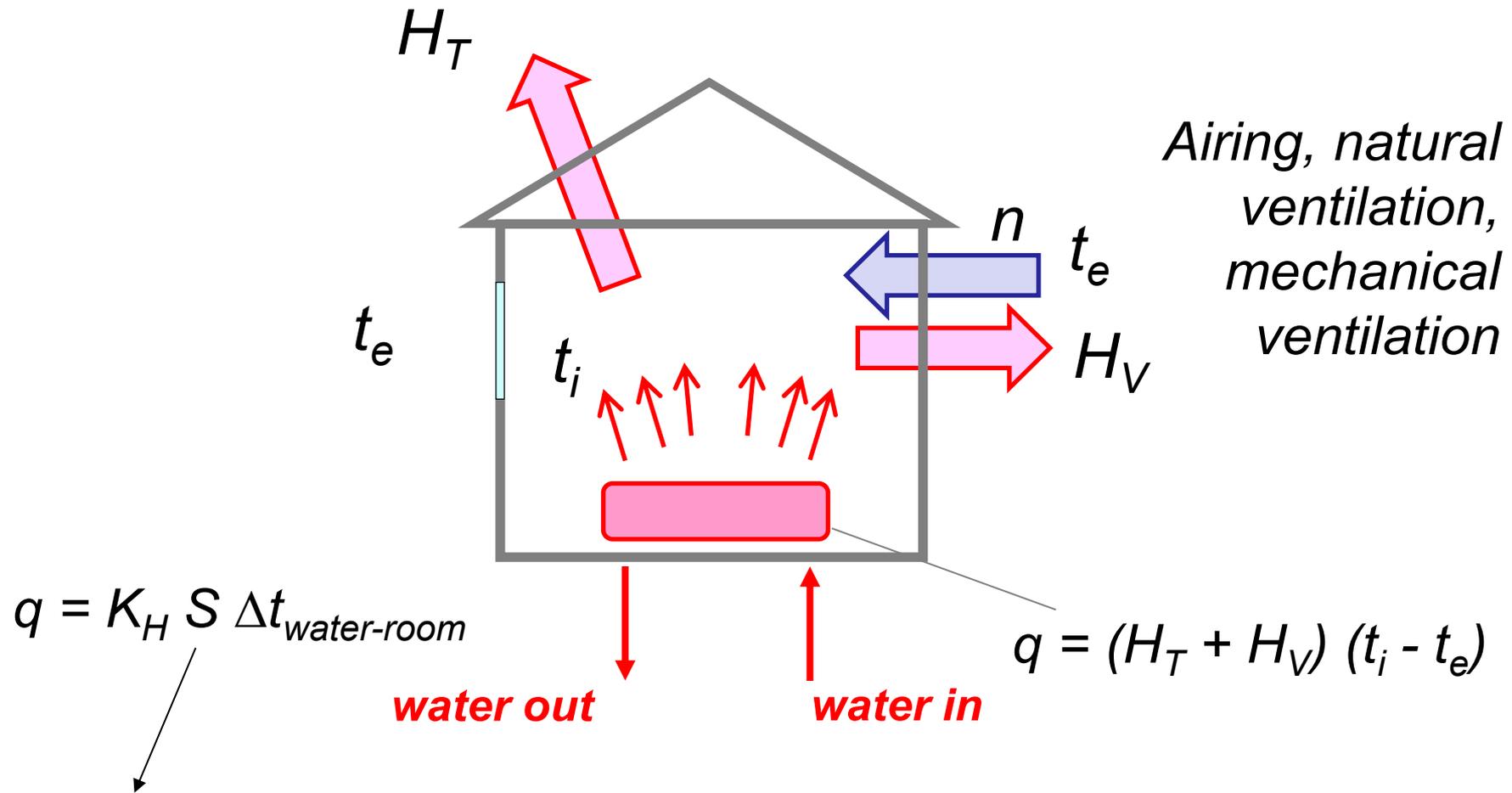


**EPBD**  
**Energy Performance**  
**Building Directive**

**Energy policy**

# Types of HVAC systems

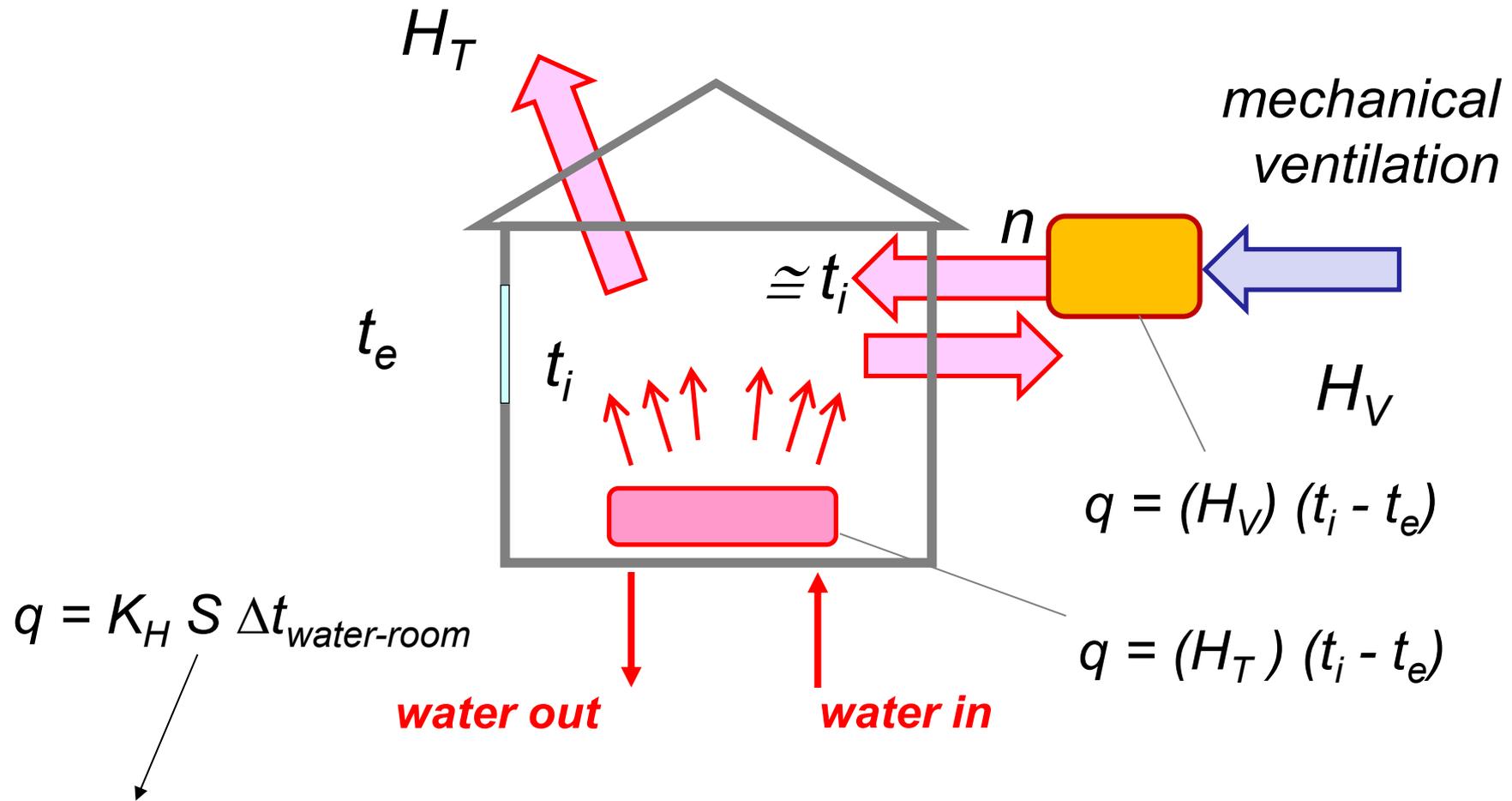
## 1. Water based heating



- Type and size of the emission system
- Average water temperature in the emission system

# Types of HVAC systems

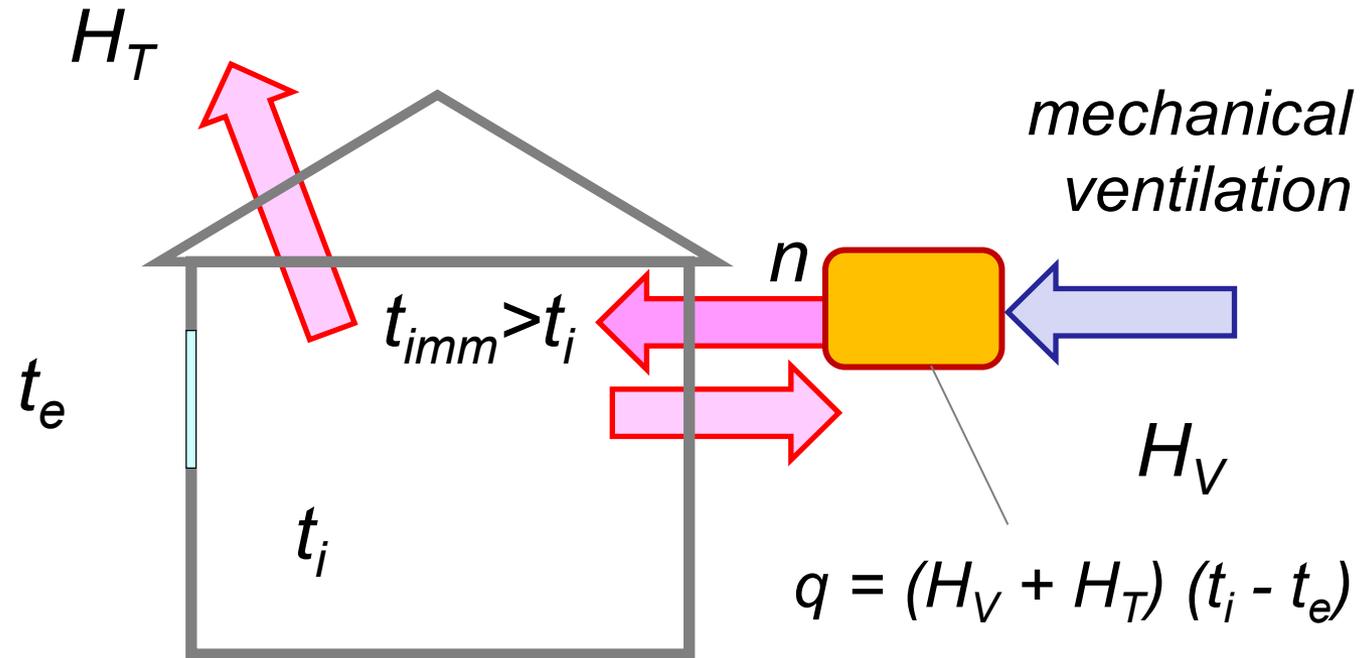
## 2. Air and water based heating



- Type and size of the emission system
- Average water temperature in the emission system

# Types of HVAC systems

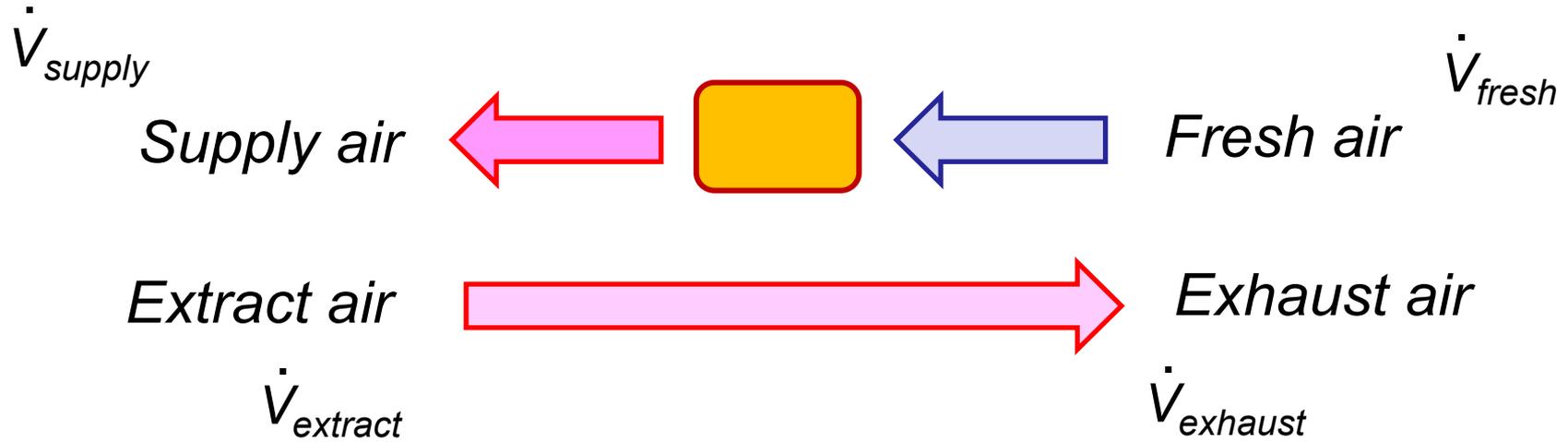
## 3. Full air heating



The air enters the room with higher temperature ( $t_{imm}$ ) than  $t_i$ . Depending on the flow rate and  $t_{imm}$ , there are 2 possible solutions.

# 1) No recirculation:

$$\dot{V}_{fresh} = \dot{V}_{supply} \cong \dot{V}_{exhaust}$$



# 2.) With recirculation:

$$\dot{V}_{fresh} < \dot{V}_{supply} \cong \dot{V}_{extract}$$

