

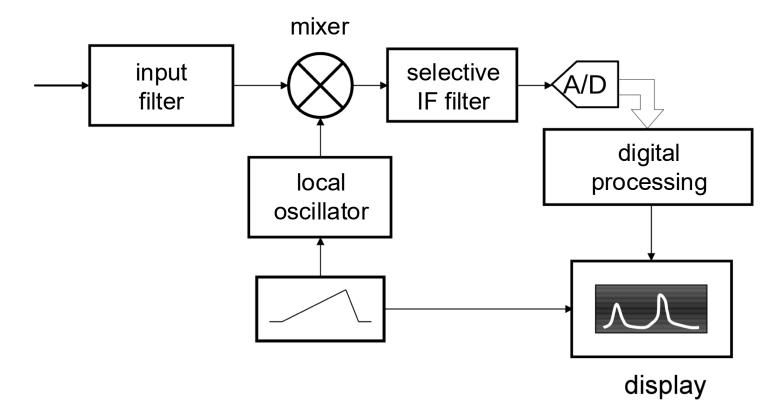
# Spectrum analyzer with digital IF

Lecture #13
Electronic measurements
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#### Sampled IF filter output

- Digital signal processing in the intermediate frequency section of a spectrum analyzer
  - High-speed, high-resolution ADCs
  - High-stability oscillators





#### Sampled IF filter output

- IF filter output spectrum  $\Rightarrow$  frequency band centred exactly on the **filter** frequency  $f_{IF}$
- Width determined by the filter resolution bandwidth
- Filter output y(t) band limited pass-band signal

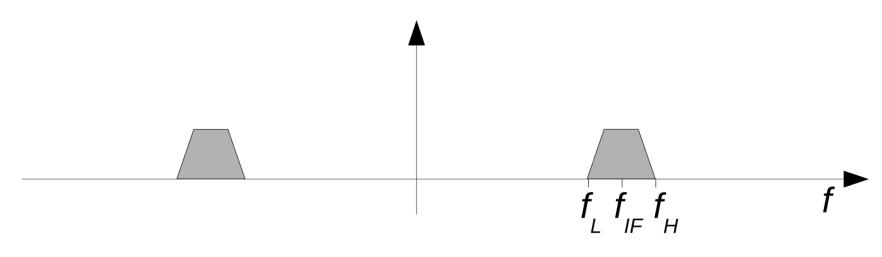


**Undersampling** 

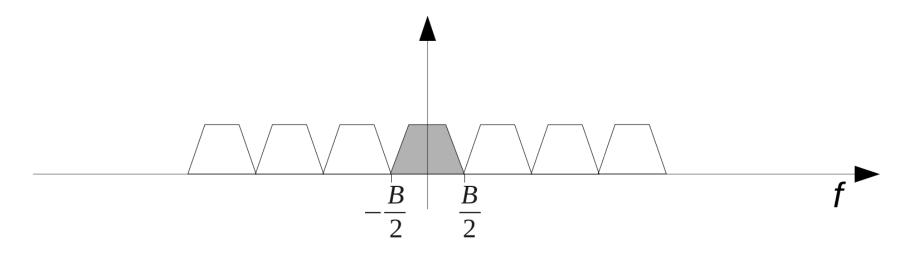
#### Undersampling

- $f_L$  and  $f_H$  lower and upper limit of the IF filter bandwidth  $\Rightarrow B = f_H f_L$
- Maximum bandwidth of the filter output y(t)
- $f_L = f_{IF} \frac{B}{2}$
- $f_H = f_{IF} + \frac{B}{2}$
- Sampling theorem:  $f_S > 2 \cdot f_H$
- For a band limited signal, however, failure to satisfy this condition does not necessarily imply a distortion of the spectrum caused by aliasing
- The periodic repetitions of the signal spectrum caused by sampling may not overlap

# Undersampling



(a) band-pass signal;



#### **Undersampling**

- $f_S > B$
- $B \ll f_H$
- $\frac{f_H}{R} = k$ , k integer  $\Rightarrow$  Condition related to IF filter design parameters
- ADC converter at the IF filter output, operating at a sampling rate determined by the IF filter bandwidth
- Traditional swept-frequency spectrum analyzer ⇒ Narrow band IF filter
- Spectrum analyzer with **digital IF section** ⇒ **Less restrictive conditions**



Accurate analysis through digital signal processing

# DEGLI STUDI DI PADOVA I-Q modulation

IF filter output:

$$y(t) = K_M \left\{ \frac{1}{2} \cos 2\pi f_{IF} t[i(t)] + \frac{1}{2} \sin 2\pi f_{IF} t[q(t)] \right\} =$$

$$= \frac{K_M}{2} \left\{ \frac{e^{j2\pi f_{IF}t} + e^{-j2\pi f_{IF}t}}{2} [i(t)] + \frac{e^{j2\pi f_{IF}t} - e^{-j2\pi f_{IF}t}}{2j} [q(t)] \right\} =$$

$$= \frac{K_M}{2} \left\{ [i(t) + jq(t)] \frac{e^{-j2\pi f_{IF}t}}{2} + [i(t) - jq(t)] \frac{e^{j2\pi f_{IF}t}}{2} \right\}$$

- i(t) + jq(t) complex base-band signal a(t)
- i(t) in-phase component
- q(t) quadrature component

# DEGLI STUDI DI PADOVA I-Q modulation

Frequency domain expression

$$Y(f) = \frac{K_M}{2} \{ [I(f - f_{IF}) + jQ(f - f_{IF})] + [I(f + f_{IF}) - jQ(f + f_{IF})] \}$$

• 
$$A(f) = I(f) + jQ(f)$$
  

$$Y(f) = \frac{K_M}{2} \{ [A(f - f_{IF})] + [A^*(f + f_{IF})] \}$$

•  $i(nT_s)$  and  $q(nT_s)$  sampled components

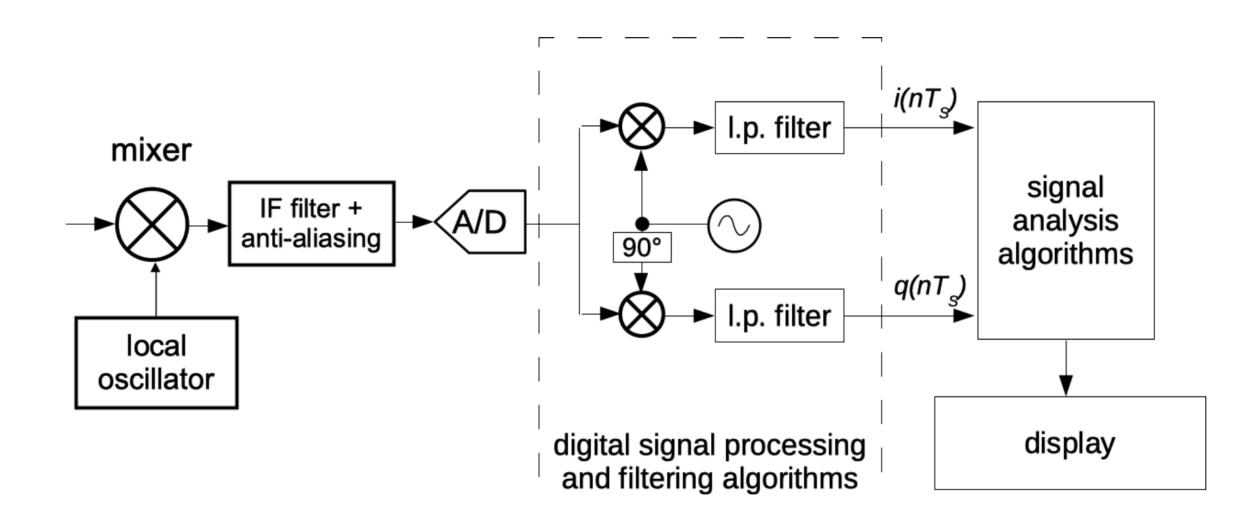
$$y(nT_S) = \frac{K_M}{2} \{\cos 2\pi f_{IF} nT_S[i(nT_S)] + \sin 2\pi f_{IF} nT_S[q(nT_S)] \}$$

#### I-Q demodulation

- $y(nT_s)$  is sent to **two multipliers in parallel**:
  - $y(nT_s) \cdot \cos 2\pi f_{DDC} nT_s$
  - $y(nT_s) \cdot \sin 2\pi f_{DDC} nT_s$
- Low-pass filtering
  - $i(nT_s) \cdot \cos 2\pi (f_{DDC} f_{IF}) nT_s$
  - $q(nT_s) \cdot \cos 2\pi (f_{DDC} f_{IF}) nT_s$
- If  $f_{DDC} = f_{IF} \Rightarrow$  Base-band components



Digital down-converter (digital demodulator)



#### Specifications and requirements

ADC converter performances

#### ADC resolution:

- Lower bound ⇒ Noise floor
- ADC signal to quantization noise ratio =  $\sim 6 \cdot b dB$
- 80 dB dynamic range  $\Rightarrow$  b = 14

#### Sampling clock stability

- Jitter: variation of the sampling instant from the nominal time
- Statistical characterization  $\sigma_t$
- Phase noise standard deviation  $\sigma_{\phi} = 2\pi f_s \sigma_t$

- Extend the range of possible measurements
- Multi-domain analysis
- Analysis of digital modulations

• **Digital IF filter** → Rather large bandwidth values



Selector for the frequency intervals of interest in a variety of radio-frequency (RF) communication systems

Within the allocated frequency intervals, high bit rate wireless technologies
occupy specified sub-bands of width in the order of some MHz

Communication channel analysis



Superheterodyne



• Frequency shift of the centre frequency of the input signal to coincide with the IF filter centre frequency

 Since analysis algorithms must be allowed to operate on the signal in its entirety, IF filter bandwidth should correspond to that of the whole channel

Large bandwidth

- Maximum value of the resolution bandwidth
  - Analysis of high data rate wireless channels
- Minimum value of the resolution bandwidth
  - Accurate measurements of spectrum

- High resolution ADC
  - Avoid aliasing  $\rightarrow$  IF filter is also a pass-band anti-aliasing filter (IF filter implementable as a multi-stage to increase out-of-band attenuation)

### VSA signal processing

- First signal processing stage
  - **Digital Down Conversion**  $\rightarrow$  baseband in-phase and quadrature components
  - Sampling decimation
- FFT analysis
- Digital demodulation algorithms
  - Modulation domain analysis
- Conversion into digital data sequences

Reference measuring receiver

## VSA signal processing

Known modulation of the received signal

- Analysis of the received signal
  - Oscilloscope: observation of in-phase and quadrature component
  - Spectrum analyzer: spectral measurements
- VSA
  - Triggering
  - Synchronization
  - Decoding

## VSA signal processing

- Performance goals in a communication system
  - Spectral efficiency → optimal use of the electromagnetic spectrum
  - Immunity to noise and interference
  - Reduced power consumption  $\rightarrow$  in particular, for wireless applications such as mobile telephony, sensor networks and Internet of Things (IoT) applications
- Modulation domain analysis is also important in wired communications
  - Broadband digital subscriber lines
  - Power line communication
  - Industrial communications

#### Vector (I-Q) diagrams

- Measured data displayed by means of two-dimensional maps referred to the in-phase and quadrature baseband signal components
- Vector Diagrams
- Complex signal  $a(nT_s) = i(nT_s) + jq(nT_s)$
- Orthogonal plane having I and Q as its axes
- Evolution over time of a vector trajectory

 Modulated signals: decomposition into two orthogonal in-phase (I) and quadrature (Q) components



Simple phase and amplitude modulation analysis

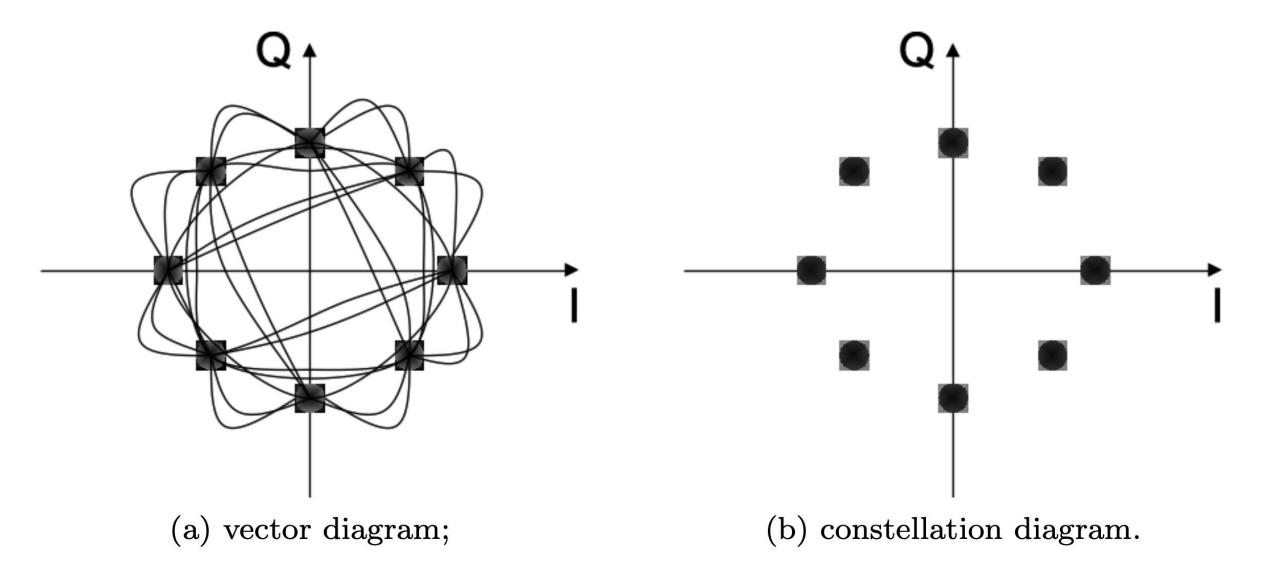
#### Vector (I-Q) diagrams

- **Vector diagram**: the whole trajectory of the complex vector representing the modulating signal is presented in its evolution over time
- Constellation diagram: the diagram presents the value of the modulating signal only at decision time, that is, when I and Q components are sampled to determine the value of the measured (received) symbol

- Other measurements:
  - Multilevel eye diagrams
  - Separate I and Q components analysis



## Vector (I-Q) diagrams



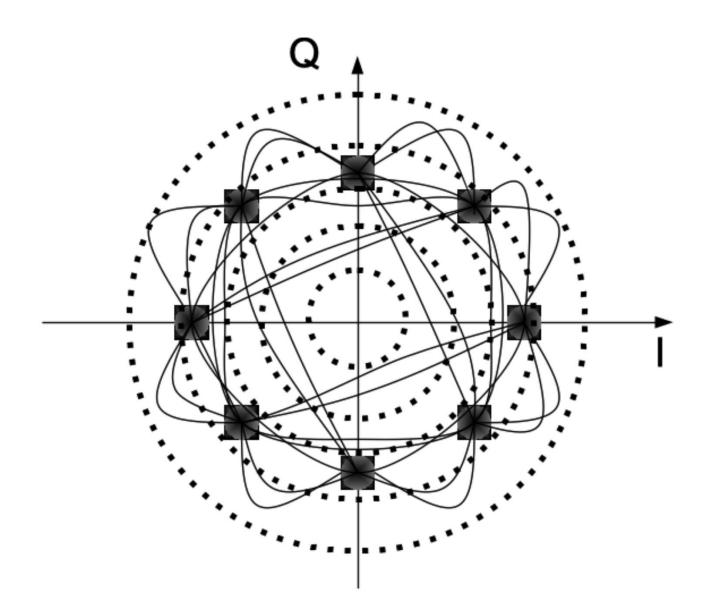
- Displays the whole vector trajectory of the modulating signal, not only at decision times, but during the whole observation interval
- Analysis of the circuit characteristics of a transmission system
  - Transitions between symbols may correspond to variations of the signal power



**Detect malfunctions or improper behaviour** (e.g., undesired power peaks during transients, low transitions...)

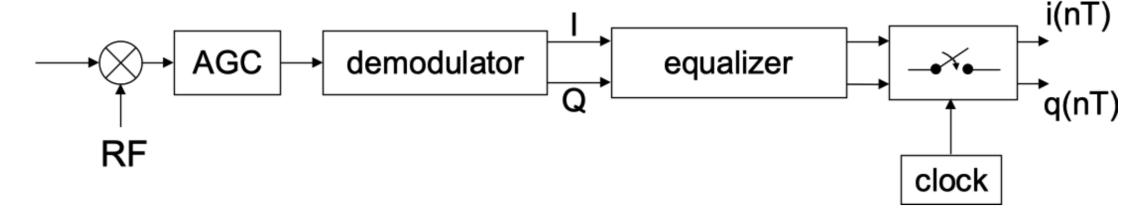
- Signal power is associated to circumferences on the I-Q plane
  - Overlayed on a vector diagram
  - Assessment of minimum and maximum power

# Vector diagram

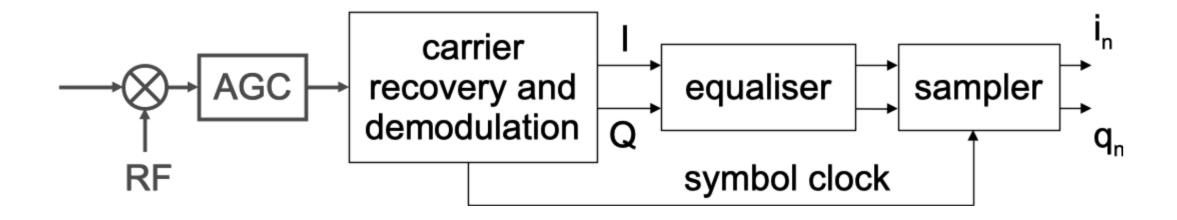


#### Receiver structure

- Automatic gain control (AGC): compensates the attenuation at the receiver input
- **Equalizer:** reproduces the reference behaviour of a receiver designed for the modulation format under analysis
  - Any deviation of the actual diagram from the expected one can be correctly attributed to some form of impairment in the transmitter/receiver system
- Clock: VSA internal sampling clock, at higher frequency and independent of the symbol clock employed in the communication system



- Constellation diagram: i(t) and q(t) have to be determined exactly at the communication system **decision times**
- The measuring system must be able to employ the same symbol clock as the system under analysis
  - Supplied as an independent input
  - Recovered from the analyzed signal, as a receiver would do





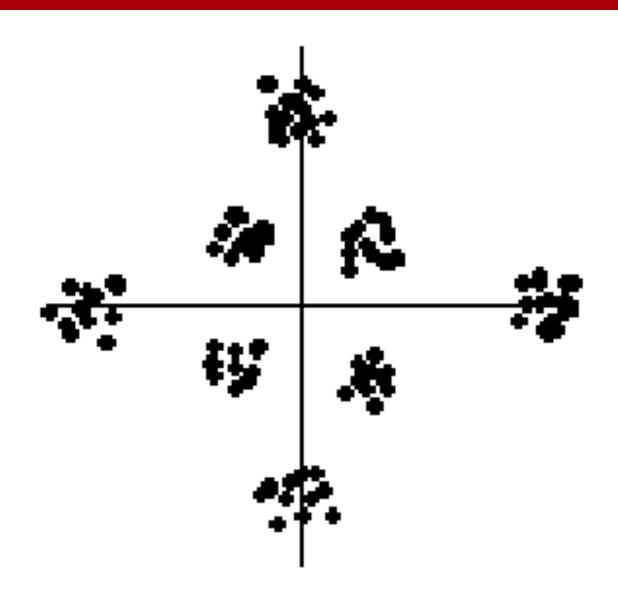
- Sampled sequences  $i(nT_s)$  and  $q(nT_s)$  are resampled at the lower symbol frequency
- Sampled baseband vector components at decision times  $\rightarrow$  **Actual values**
- Compared to the nominal values (references)

- Presence of broadband noise
- Actual and nominal values do not perfectly coincide



**Creation of clusters** 

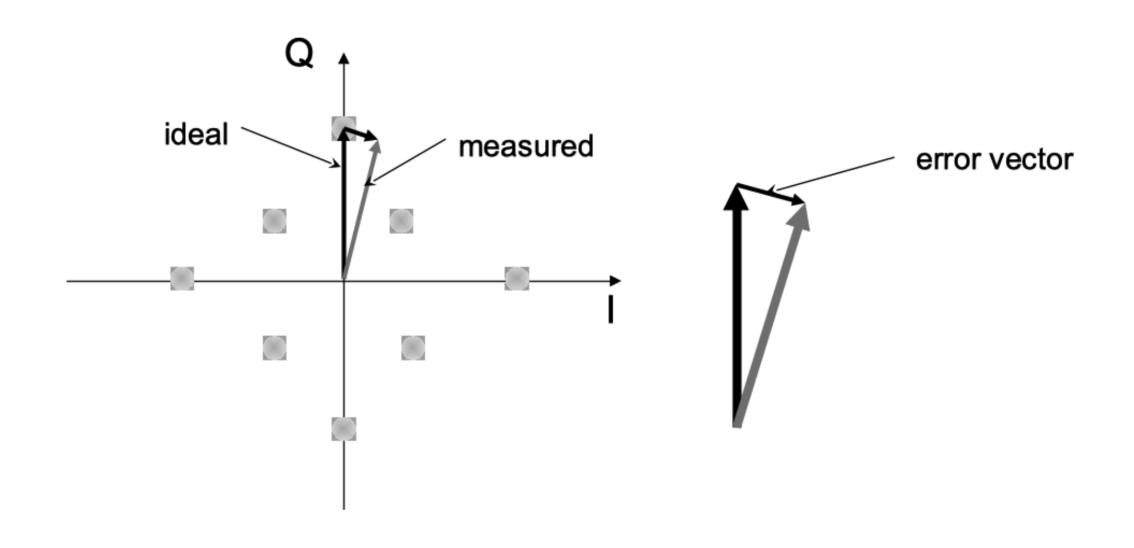




- Correct operation: the dispersion of measured points will only be due to the effect of noise on the measuring receiver
- Noise power estimation
- Assessment of Signal-to-Noise Ratio (SNR)

- Deviations from the nominal constellation points → Error vector
- **Difference in the I-Q plane** between the actual measured vector position and its ideal position in the nominal reference constellation





#### **Error vector determination**

- The measuring instrument associates the measured point to a specific constellation symbol
  - The measured coordinates  $i_m$  and  $q_m$  are sent to a decision element called slicer
  - The slicer determines the region of the I-Q plane where the measured point falls and assigns the reference constellation symbol accordingly
- The measured symbol  $\underline{\hat{a}}_m=\hat{\imath}_m+j\hat{q}_m$  is then compared to the reference symbol  $a_{ref}$
- The error vector is calculated

$$\underline{e}_m = \underline{\hat{a}}_m - \underline{a}_{ref}$$

#### Parameters of interest

Noise power:

$$\hat{\sigma}_e^2 = \frac{1}{M} \sum_{m=1}^M \left| \underline{e}_m \right|^2$$

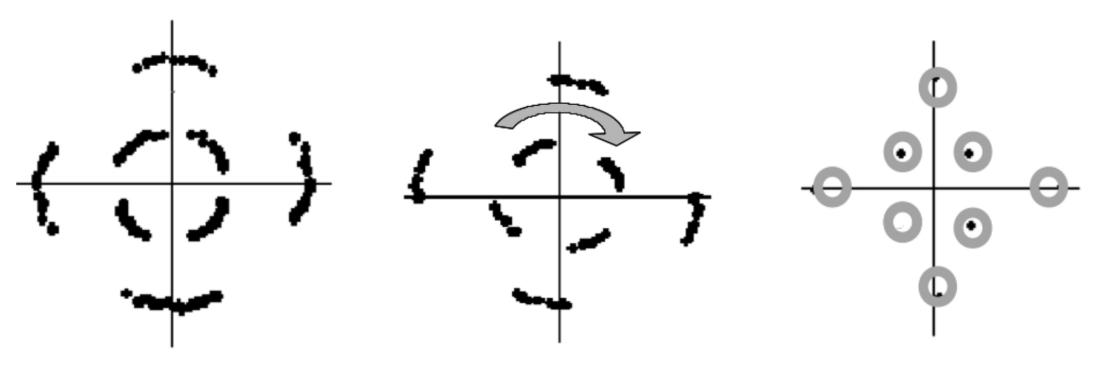
where M is the number of symbols acquired during the measurement interval

• Analysis of an individual cluster  $C_a$ :

$$\sigma_a = \sqrt{\frac{1}{M_a} \sum_{\underline{\hat{a}}_m \in C_a} |\underline{e}_m|^2}$$

- Cluster extension
- "Closure" for a specific symbol  $\rightarrow \sigma_a/(d/2)$  where d is is the distance between contiguous symbols

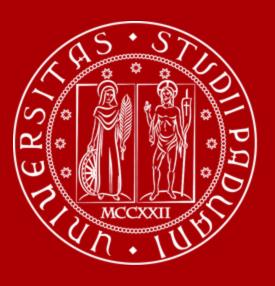
Direct evidence of some kinds of system performance impairment



(a) jitter: "vibration" around nominal position;

(b) frequency offset: "rotation" in the I-Q plane;

(c) sinusoidal interferer.



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