

# Domestic Hot Water production

HEATING VENTILATION AIR CONDITIONING SYSTEMS

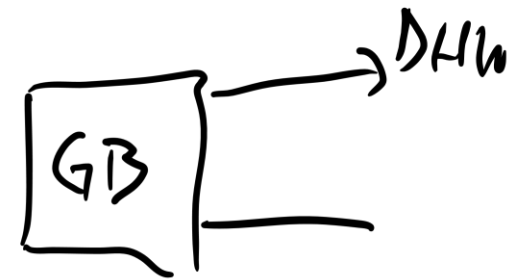
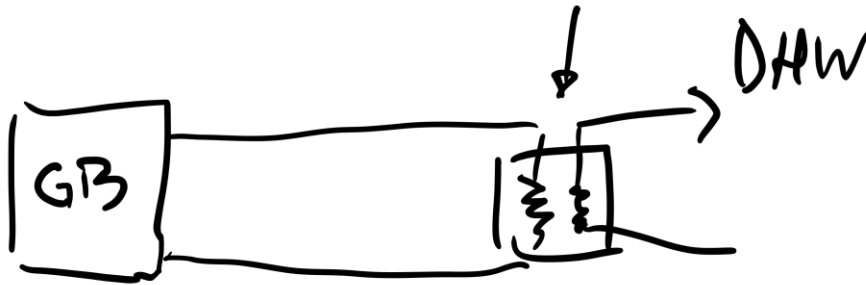
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# Classification of systems

## Direct vs indirect production

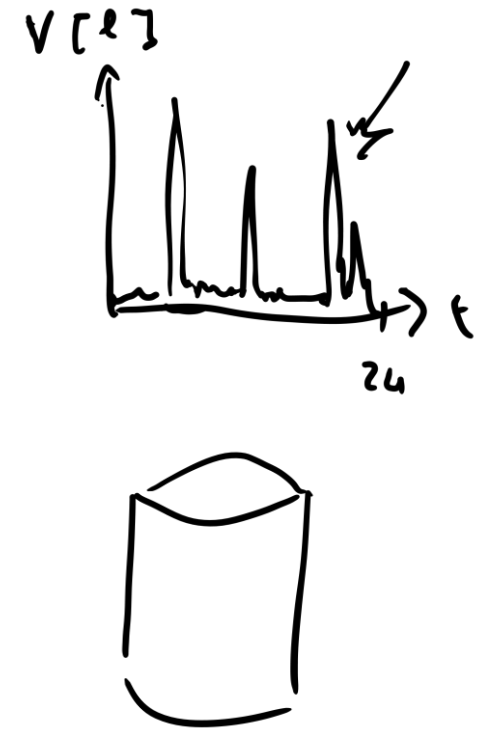
- **Direct:** DHW is produced inside the heat generation (e.g. heat pump or gas boiler)
- **Indirect:** there is an intermediate heat exchanger between heat generation and DHW circuit



# Classification of systems

## Instantaneous systems vs systems with storage

- **Instantaneous:** heat generation (e.g. heat pump or gas boiler) supplies heat for DHW production to the users instantaneously (either direct or indirect)
- **With storage:** heat generation (e.g. heat pump or gas boiler) supplies heat to a thermal storage tank, which supplies heat to the users when needed (either direct or indirect)



# Instantaneous production

## **Example**

Single family house with 2 baths: 1 shower and 1 sink each.

Sinks: 2 (baths) + 1 (kitchen) + 1 (laundry) + 1 (bidet) = 5

Showers: 2 (baths)

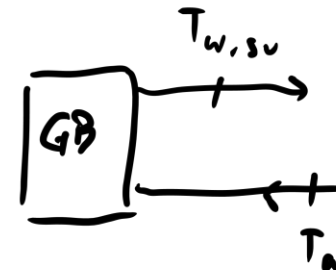
Assume 6 l/min for sinks and 12 l/min for showers

# Instantaneous production

## Example

Single family house with 2 baths: 1 shower and 1 sink each.

$$\dot{Q}_{V, \max} = 2 \cdot 12 + 5 \cdot 6 = 54 \text{ l/min} = 0.9 \text{ l/s} \rightarrow \dot{m} = 0.9 \text{ kg/s}$$
$$q = \dot{m} c_p (T_{w, \text{su}} - T_a) = 0.9 \cdot \frac{\text{kJ}}{\text{kg K}} (40 - 10) = 113 \text{ kW}$$



↳ unrealistic → oversizing

# Instantaneous production

## Example

Single family house with 2 baths: 1 shower and 1 sink each.

$$12 \text{ l/min}$$

↓

$$\frac{12}{60} \text{ m}^3/\text{s}$$

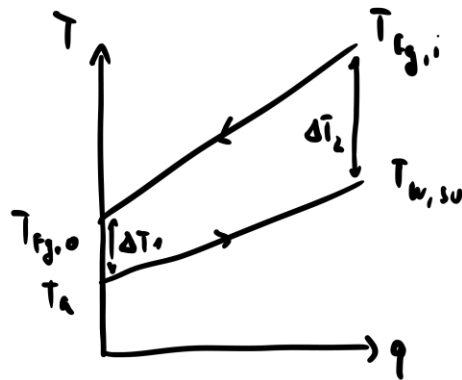
$$q = 0.2 \cdot 4.18 (40 - 10) \approx 25 \text{ kW}$$

$$\boxed{q \approx 30 \text{ kW}} \quad \text{SH} + \underline{\underline{\text{DHW}}}_{\text{prod.}}$$

# Instantaneous production

## Heat source

Flue gases from gas boilers or hot water produced with heat pumps.



$$q_{\text{peak}, \text{SHW}} > q_{\text{peak}, \text{SH}}$$

$$\Delta T_1 = T_{fg,o} - T_a$$

$$\Delta T_2 = T_{fg,i} - T_{w,su}$$

$$\Delta T_{m1} = \frac{\Delta T_1 - \Delta T_2}{\ln \frac{\Delta T_1}{\Delta T_2}}$$

$$S = \frac{q}{K \cdot \Delta T_{m1}}$$

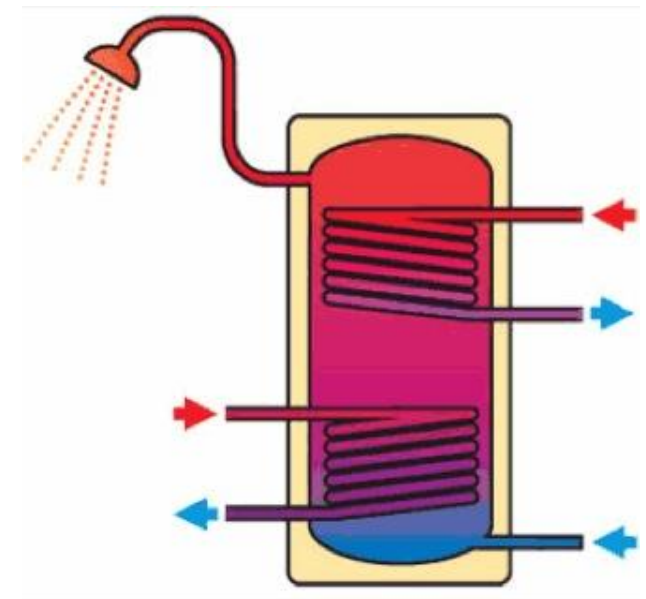
flue-gases  
water

$$q = K S \cdot \Delta T_{m1}$$

# Systems with storage

## Classification of systems with storage

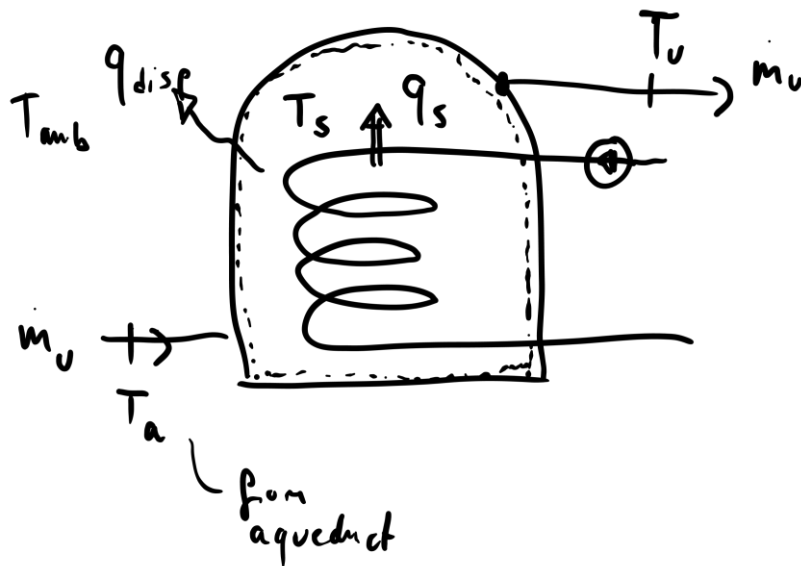
- **Mixed hot water tank:** the water in the tank is the domestic hot water (*accumulo a miscela*)
- **Thermal storage:** the water in the tank is technical water which heats up the domestic hot water through a coil (thermo-*accumulo*)





# Mixed hot water storage

## Energy balance



$$q_s - q_{\text{disp}} = m_u h_v - m_u h_a + \frac{dU_{\text{stor}}}{dz} + \phi$$

$$q_s - \underbrace{UA}_{\text{walls}} (T_s - T_{\text{amb}}) = m_u c_p (T_v - T_a) + \underline{\underline{m_s c_v}} \frac{dT_s}{dz}$$

Uniform temp. in storage  $T_v = T_s$

$$c_p = c_v = c = 4.186 \frac{\text{kJ}}{\text{kg} \cdot \text{K}}$$

# Mixed hot water storage

## Energy balance

$$q_s - UA(\bar{T}_s - T_{amb}) = m_u c (\bar{T}_s - T_a) + \rho_w V_s c \frac{d\bar{T}_s}{dt}$$

$$\rho_w V_s c \frac{d\bar{T}_s}{dt} + \bar{T}_s (m_u c + UA) = q_s + UA \cdot T_{amb} + m_u c T_a$$

$$\rightarrow \frac{d\bar{T}_s}{dt} + \underbrace{\bar{T}_s \left( \frac{m_u c + UA}{\rho_w V_s c} \right)}_a = \underbrace{\frac{q_s + UA \cdot T_{amb} + m_u c T_a}{\rho_w V_s c}}_b$$

$$\rightarrow \frac{dy(t)}{dt} + a y(t) = b$$

$$y(t) = \frac{b}{a} + C e^{-at}$$

— sizing  
— demand  
of the  
user

# Mixed hot water storage

## Energy balance

$$q_s - UA(\bar{T}_s - T_{amb}) = \dot{m}_u c (\bar{T}_s - T_a) + \rho_w V_s c \frac{d\bar{T}_s}{dt}$$

$$\rho_w V_s c \frac{dT_s}{dt} + T_s (\dot{m}_u c + UA) = q_s + UA \cdot T_{amb} + \dot{m}_u c T_a$$

$$\rightarrow \frac{dT_s}{dt} + T_s \underbrace{\left( \frac{\dot{m}_u c + UA}{\rho_w V_s c} \right)}_a = \underbrace{\frac{q_s + UA \cdot T_{amb} + \dot{m}_u c T_a}{\rho_w V_s c}}_b$$

$$\rightarrow \frac{dy(t)}{dt} + a y(t) = b$$

$$y(t) = \frac{b}{a} + C e^{-at}$$

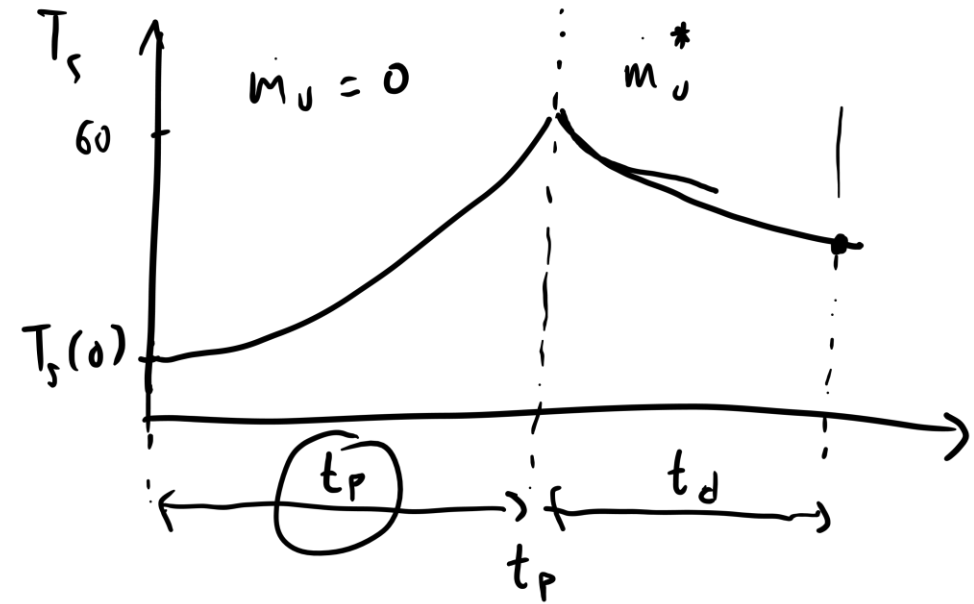
— sizing  
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# Mixed hot water storage

## Energy balance

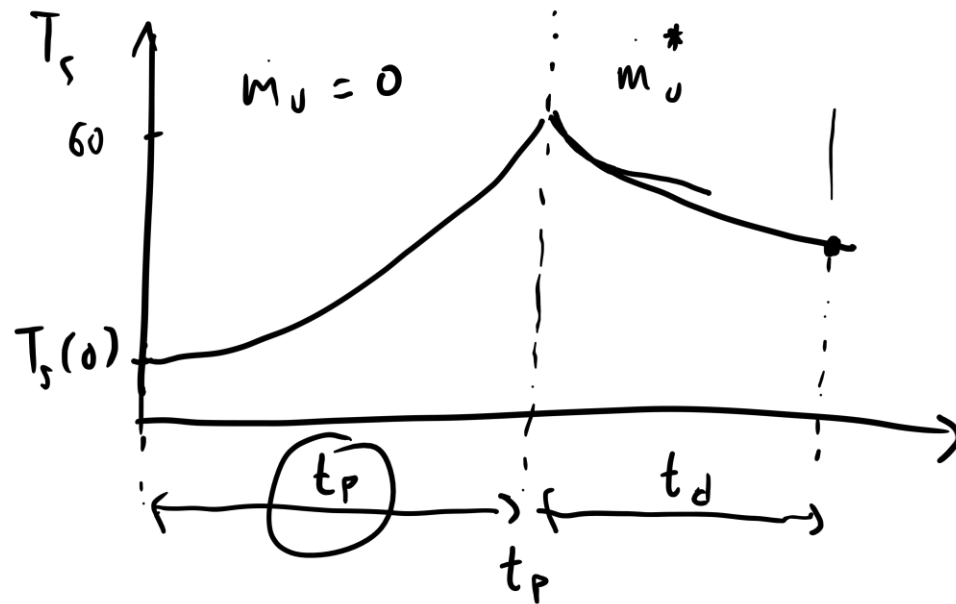
$$\begin{cases} \bar{T}_s(t) = \frac{b}{a} + C e^{-at} \\ T_s(t=0) = \frac{b}{a} + C \end{cases} \rightarrow C = T_s(0) - \frac{b}{a}$$

$$T_s(t) = \frac{b}{a} + \left( T_s(0) - \frac{b}{a} \right) e^{-at}$$



# Mixed hot water storage

## Energy balance



$m_u = 0$  Pre-heating

$m_u \leftarrow ?$  Delivery

Pre-heating  $a = a_p$   $b = b_p$  ( $m_u = 0$ )

Delivery  $a = a_d$   $b = b_d$  ( $m_u^*$ )

# Mixed hot water storage

## Sizing

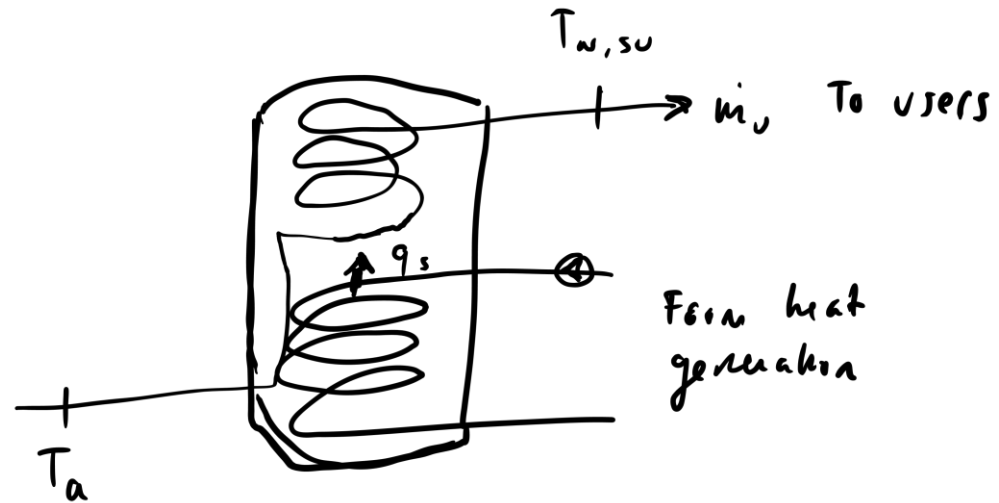
Fix pre-heating time ( $t_p$ ) and delivery time ( $t_d$ )



find hot water storage volume ( $V_s$ ) and thermal power of the coil ( $q_s$ )

# Thermal storage

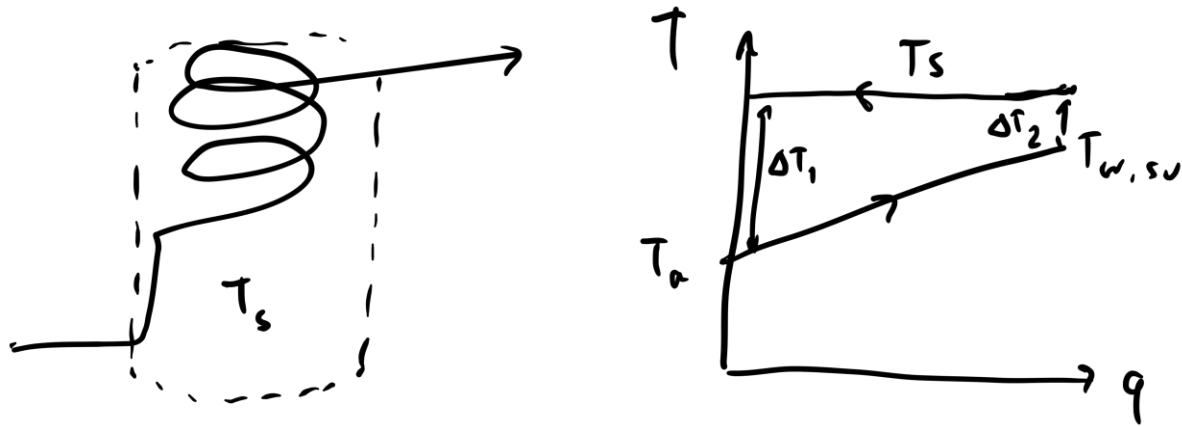
## Energy balance



$$q_s - UA(T_s - T_{amb}) = m_u c (T_{w,su} - T_a) + m_s c \frac{dT_s}{dt}$$

# Thermal storage

## Energy balance



$$q_{st \rightarrow w} = \dot{m}_v c_p (T_{w,su} - T_a)$$

$$q_{st \rightarrow w} = KS \frac{T_{w,su} - T_a}{\ln \frac{T_s - T_a}{T_s - T_{w,su}}}$$

$$\dot{m}_v c (\cancel{T_{w,su} - T_a}) = KS \frac{\cancel{T_{w,su} - T_a}}{\ln \frac{T_s - T_a}{T_s - T}}$$

$$\ln \frac{T_s - T_a}{T_s - T_{w,su}} = \frac{KS}{\dot{m}_v c}$$



# Thermal storage

## Energy balance

$$\frac{T_s - T_a}{T_s - T_{w,su}} = e^{\frac{KS}{m_u c}} \quad T_{w,su} = f(T_s) \quad \left[ \begin{array}{l} \text{for mixed hot} \\ \text{water st: } T_u = T_s \end{array} \right]$$

$$\hookrightarrow T_{w,su} = T_s - (\bar{T}_s - T_{w,e}) e^{\frac{-KS}{m_u c}} \quad \leftarrow$$

$$q_s - UA(\bar{T}_s - T_{amb}) = m_u c (T_{w,su} - T_a) + m_s c \frac{d\bar{T}_s}{dt}$$

—

# Thermal storage

## Sizing

Fix pre-heating time ( $t_p$ ) and delivery time ( $t_d$ )



find hot water storage volume ( $V_s$ ) and thermal power of the coil ( $q_s$ )

# Operating temperature

## **The problem of legionella**

Legionella is an aerobic bacterium that grows in warm (20-50°C) aquatic habitats.

It is a problem in case of stagnating water → mixed hot water storage systems.

# Operating temperature

## **The problem of legionella**

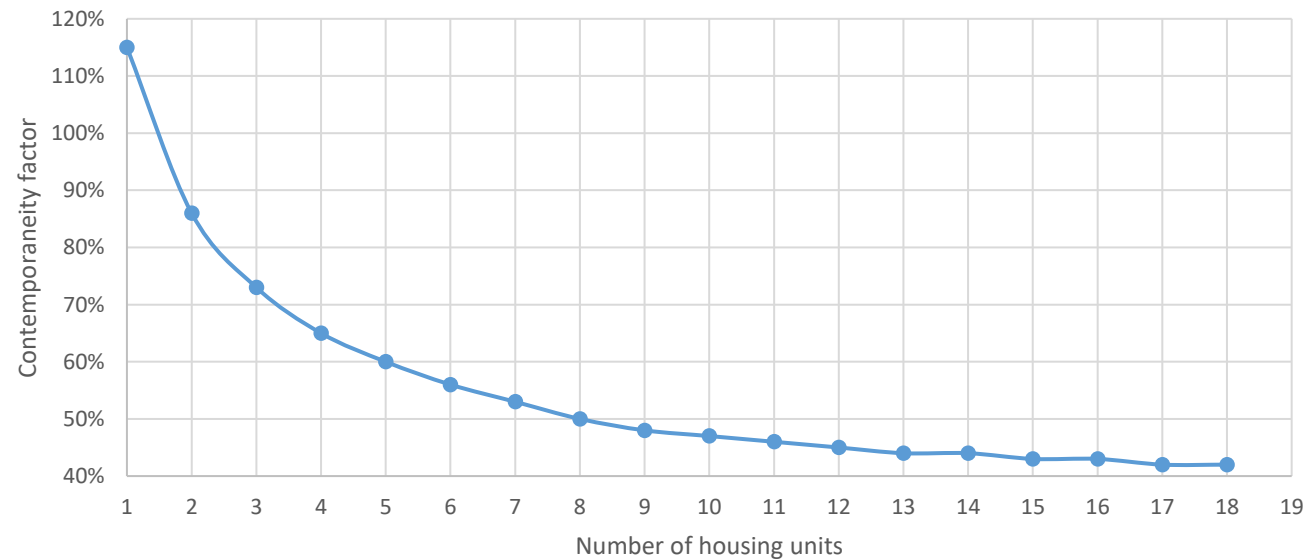
Can be prevented by:

- Avoiding stagnation
- Keeping  $T_s > 60^{\circ}\text{C}$  (threshold depending on the Standard)
- Thermal shocks or anti-legionella cycles (bringing  $T_s$  to  $70\text{-}80^{\circ}\text{C}$  every day for 30 minutes)
- Hyper-cloarting hot water (disinfecting action)

# Sizing for multiple units

## Contemporaneity factor

Users do not ask for DHW exactly in the same moment



# Integration of renewables

## Solar heat

Heat from solar collectors into systems with storage

