

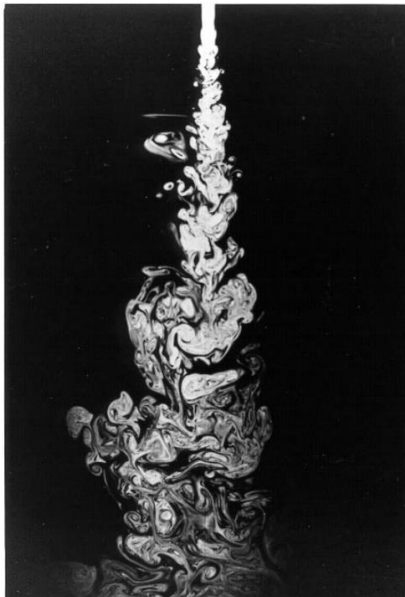
LESSON 1: INTRODUCTION TO THE COURSE

Program of the course:

- Transport dynamics of solute:

- Advection/Convection
- Diffusion
- Dispersion

} Main mechanisms



*Turbulence mixing of jet-fluid
(Dimotakis, 1993)*



Confluence of the Green and Colorado Rivers

- Solute/pollutant dynamics in rivers: - conservative solute
- non-conservative pollutants



Red dye in river



River eutrophication

- Salt wedge and density currents



Density current intrusion in a saline coastal ambient. (Photo: I. Wood, Univ. of Canterbury)

Main objectives of the course:

- Analyzing pollutants transport mechanisms
- Estimating pollutants/chemical concentrations to determine water quality
- Using advection-dispersion models to analyze future scenarios

Preliminary knowledge.

- Fluid properties: fluid density, dynamic and kinematic viscosity,...
- Continuity equation and Principle of conservation of Energy and Momentum
- Momentum equation of real fluid (Navier-Stokes equation)
- Non-dimensional parameters (Reynolds number, Froude number, etc..)
- Basic principles of open channel flow (uniform flow, supercritical and subcritical flow,...)

Suggested textbook

- White, F. M. (1979). *Fluid mechanics*. Tata McGraw-Hill Education.

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Reference texts:

- S. Lanzoni. Dinamica degli inquinanti nei corpi idrici superficiali. *Lecture notes*.
- Snoor, J. L. (1996). Environmental Modelling, Fate and Transport of Pollutants in Water, Air, and Soil. *John Wiley & Son Ltd*.
- Rutherford, J. C. (1994). River mixing. *John Wiley & Son Ltd*.
- Fischer, H. B., List, J. E., Koh, C. R., Imberger, J., & Brooks, N. H. (2013). Mixing in inland and coastal waters. *Elsevier*.
- Pedersen, F. B. (2012). *Environmental Hydraulics: Stratified Flows* (Vol. 18). Springer Science & Business Media.
- PPTs of the lectures.

About the exam

Oral exam: 1st question (>6/10)
 2nd question (>6/10)
 group exercises (>6/10)

*concerning the course
experimental activities*

Date:	I exam session:	01/02/2023	9.00 a.m.	room IP
	II exam session:	14/02/2023	9.00 a.m.	room IP
	III exam session:	20/07/2023	9.00 a.m.	room IP
	IV exam session:	05/09/2023	9.00 a.m.	room IP

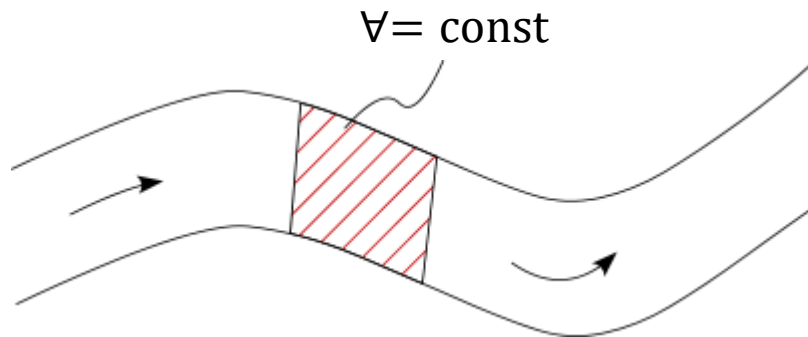
*These date may
change...*

Fluid (intensive) property ψ does not depend by the fluid mass and it can be:

- Scalar: T , ρ , ...
- Vector: $\mathbf{u}$, ...

Kinematic approach

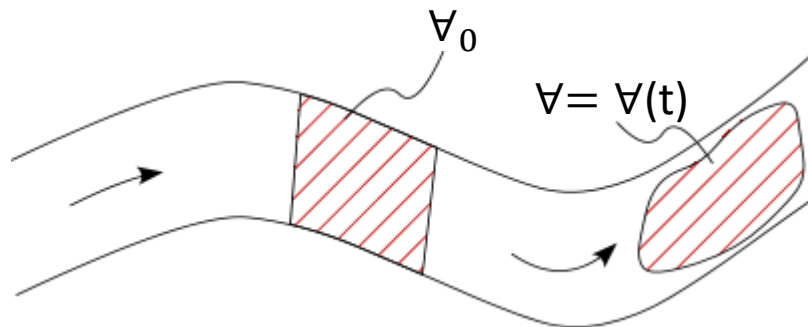
- Eulerian



Euler studies the field properties in a "fixed" domain ($\mathbf{x}$)

$$\mathbf{u} = \mathbf{u}(\mathbf{x}, t)$$

- Lagrangian



Lagrange studies the properties of the same fluid particles (ξ) which are moving along the domain

$$\mathbf{u} = \mathbf{u}(\xi, t)$$

Extensive property of fluid is: $\Psi = \int_{\forall_s} \psi \cdot d\forall$

$\forall_s$ is the System Volume or Material Volume $\longrightarrow$ Conservation of Ψ in $\forall_s$ (it is Lagrangian!)

Usually, we work on Control Volume (CV) (It is Eulerian!)

$\hookrightarrow$ How can we study Ψ in CV?

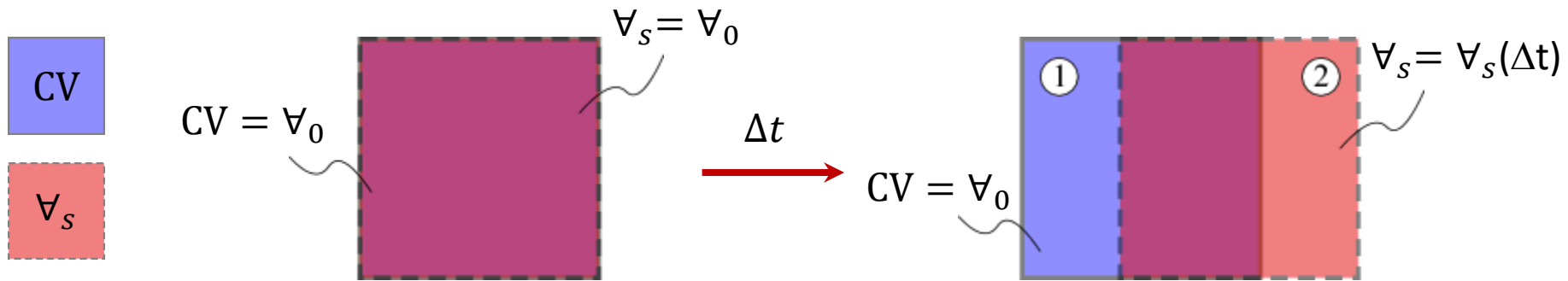
N.B.: Physics experiences are applied to System Volume and not to Control Volume

$$\sum \mathbf{F} = m \cdot \mathbf{a}$$

System Volume

$$\sum \mathbf{F} \neq m \cdot \mathbf{a}$$

Control Volume



- $t=0$ $\Psi_{V_s}(0) = \Psi_{V_0}(0)$
- $t=\Delta t$ $\Psi_{V_s}(\Delta t) = \Psi_{V_0}(\Delta t) - \Psi_1(\Delta t) + \Psi_2(\Delta t)$

By subtracting the two expressions and for $\Delta t \rightarrow 0$, we have:

$$\frac{\Psi_{V_s}(\Delta t) - \Psi_{V_s}(0)}{\Delta t} = \frac{\Psi_{V_0}(\Delta t) - \Psi_{V_0}(0)}{\Delta t} - \psi_1 \frac{\Delta V}{\Delta t} + \psi_2 \frac{\Delta V}{\Delta t}$$

$$\longrightarrow \underbrace{\frac{d\Psi}{dt}}_{\text{Lagrangian}} = \underbrace{\frac{\partial \Psi}{\partial t} - \dot{\psi}_1 + \dot{\psi}_2}_{\text{Eulerian}}$$

$$\frac{d\Psi}{dt} = ?$$

$$\frac{d\Psi}{dt} = \frac{d}{dt} \int_{V(t)} \psi \frac{dV_0}{dV_0} dV = \frac{d}{dt} \int_{V_0} \psi J dV_0$$

$$\frac{dV}{dV_0} = \det \begin{bmatrix} \frac{\partial x_1}{\partial X_1} & \frac{\partial x_1}{\partial X_2} & \frac{\partial x_1}{\partial X_3} \\ \frac{\partial x_2}{\partial X_1} & \frac{\partial x_2}{\partial X_2} & \frac{\partial x_2}{\partial X_3} \\ \frac{\partial x_3}{\partial X_1} & \frac{\partial x_3}{\partial X_2} & \frac{\partial x_3}{\partial X_3} \end{bmatrix} = J$$

$$\frac{d\Psi}{dt} = \int_{V_0} \frac{d}{dt} (\psi J) dV_0 = \int_{V_0} \left(\frac{d\psi}{dt} J + \frac{dJ}{dt} \psi \right) dV_0$$

$$\frac{d\Psi}{dt} = \int_{V_0} \left(\frac{d\psi}{dt} + \psi \nabla \cdot \mathbf{u} \right) J dV_0 = \int_{V(t)} \left(\frac{d\psi}{dt} + \psi \nabla \cdot \mathbf{u} \right) dV \quad \frac{dJ}{dt} = J \nabla \cdot \mathbf{u}$$

Let's rearrange the integrating expression

$$\frac{d\psi}{dt} + \psi \nabla \cdot \mathbf{u} = \frac{\partial \psi}{\partial t} + \mathbf{u} \cdot \nabla \psi + \psi \nabla \cdot \mathbf{u} = \frac{\partial \psi}{\partial t} + \nabla \cdot (\psi \otimes \mathbf{u}) \quad \mathbf{a} \otimes \mathbf{b} = \begin{bmatrix} a_1 b_1 & a_1 b_2 & a_1 b_3 \\ a_2 b_1 & a_2 b_2 & a_2 b_3 \\ a_3 b_1 & a_3 b_2 & a_3 b_3 \end{bmatrix}$$

$$\frac{d}{dt} \int_{\forall} \psi \, d\forall = \int_{\forall} \frac{\partial \psi}{\partial t} \, d\forall + \int_{\forall} \nabla \cdot (\psi \otimes \mathbf{u}) \, d\forall$$

Gauss th.: $\int_{\forall} \nabla \cdot \boldsymbol{\varphi} \, d\forall = \int_S \boldsymbol{\varphi} \cdot \mathbf{n} \, dS$

$$\frac{d}{dt} \int_{\forall} \psi \, d\forall = \int_{\forall} \frac{\partial \psi}{\partial t} \, d\forall + \int_S (\psi \otimes \mathbf{u}) \cdot \mathbf{n} \, dS$$

$(\mathbf{a} \otimes \mathbf{b}) \cdot \mathbf{c} = (\mathbf{b} \cdot \mathbf{c}) \mathbf{a}$

$$\longrightarrow \underbrace{\frac{d}{dt} \int_{\forall} \psi \, d\forall}_{\text{Total variation of } \psi} = \underbrace{\int_{\forall} \frac{\partial \psi}{\partial t} \, d\forall}_{\text{Local variation of } \psi} + \underbrace{\int_S \psi \mathbf{u} \cdot \mathbf{n} \, dS}_{\text{Flux across } S \text{ of } \forall}$$

Some definitions:

- Volumetric Concentration: $c_s = \lim_{\delta V \rightarrow 0} \frac{\delta M_s}{\delta V}$ [kg/m³]

M_s is the mass of solute in the fluid volume V

N.B. With more solutes: $c_s = \sum_i c_{s,i}$

- Mass Concentration: $\hat{c}_s = \lim_{\delta V \rightarrow 0} \frac{\delta M_s}{\delta M}$ [%]

M is the fluid mass in V

- Fluid Density: $\rho = \lim_{\delta V \rightarrow 0} \frac{\delta M}{\delta V}$ [kg/m³]

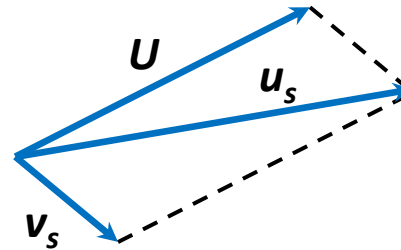
N.B.: $\hat{c}_s = \frac{c_s}{\rho}$

- Mixture Velocity (water + solute):

U : mean velocity of the mixture

v_s : diffusive velocity of the solute

u_s : absolute velocity of the solute



- Mass Flux:

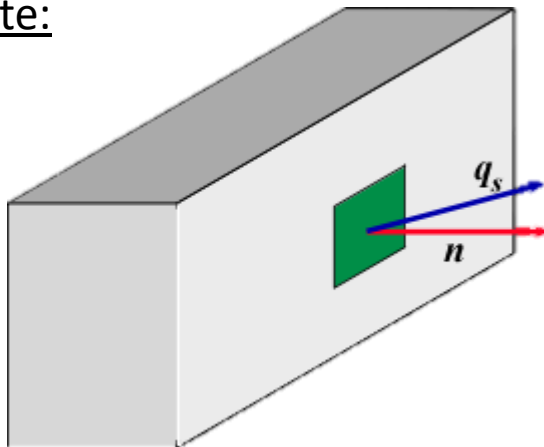
$$q_s = c_s u_s \quad [\text{kg/m}^2\text{s}]$$

N.B. With more solutes: $q_s = \sum_i q_{s,i}$

- Relative Mass Flux:

$$q_s^r = c_s (u_s - U) = c_s v_s \quad [\text{kg/m}^2\text{s}]$$

- Mass Rate:

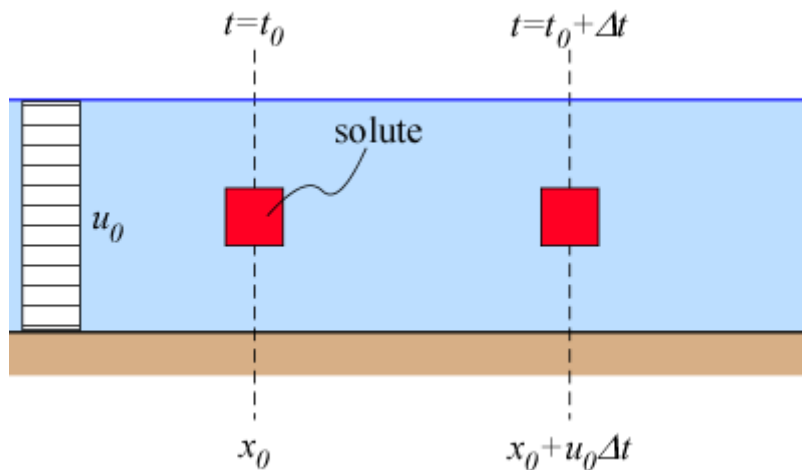


$$Q_s = \int_A q_s \cdot n \, dA \quad [\text{kg/s}]$$

1. Advection/convection

Advection: transport of a solute by the fluid

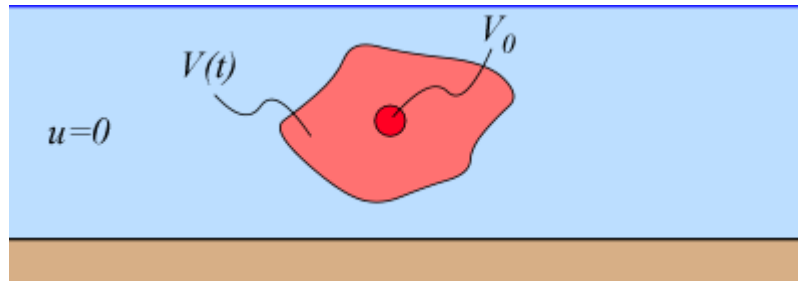
Convection: transport of an intrinsic property of fluid (e.g., momentum and temperature)



Hp: - 1D flow
- Uniform flow: $\mathbf{u}(x, t) = u_0$
- Inviscid fluid: $\mu = 0$

 Solute translate with constant velocity

2. Diffusion



Molecular Diffusion (or Brownian Motion)

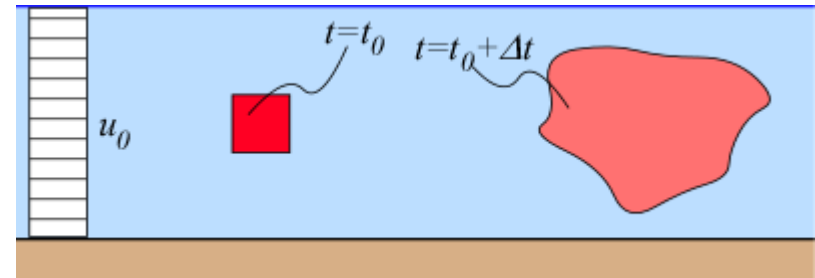


Random spreading out of molecules
due to thermodynamics condition

Turbulent Diffusion

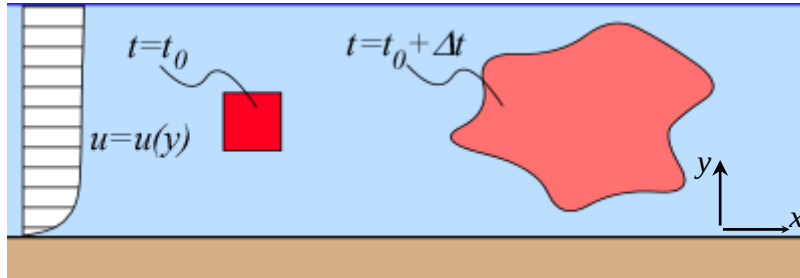


Solute spreads cause of velocity
fluctuation due to turbulence



N.B.: Turbulent Diffusion is 2 orders of magnitude greater than Molecular Diffusion

3. Dispersion



Hp: - real fluid: $\mu \neq 0$

$$\tau = \mu \frac{du}{dy}$$

→ Velocity gradient and turbulent diffusion promote the dispersion of the solute

N.B.: Dispersion is much greater than turbulent Diffusion